

" ΕΕΝ ΦΡΑΓΜΑΤΟΣ ΠΟΤΑΜΩΝ ΑΜΑΡΙΟΥ "

ΤΕΧΝΙΚΟΣ ΣΥΜΒΟΥΛΟΣ ΓΙΑ ΤΗΝ ΕΠΙΚΑΙΡΟΠΟΙΗΣΗ ΤΗΣ
ΠΡΟΜΕΛΕΤΗΣ ΚΑΙ ΤΗ ΣΥΝΤΑΞΗ ΤΩΝ ΤΕΥΧΩΝ ΔΗΜΟΠΡΑΤΗΣΗΣ
ΜΕΛΕΤΗΣ - ΚΑΤΑΣΚΕΥΗΣ ΤΟΥ ΕΡΓΟΥ
"ΕΓΚΑΤΑΣΤΑΣΗ ΕΠΕΞΕΡΓΑΣΙΑΣ ΝΕΡΟΥ ΦΡΑΓΜΑΤΟΣ
ΠΟΤΑΜΩΝ ΑΜΑΡΙΟΥ

ΘΕΜΑ ΣΧΕΔΙΟΥ:

ΜΟΝΑΔΑ ΔΙΥΛΙΣΗΣ
ΣΤΑΤΙΚΟΙ ΥΠΟΛΟΓΙΣΜΟΙ

ΑΡΙΘΜΟΣ ΣΧΕΔΙΟΥ: CA-05-ST-01

ΚΛΙΜΑΚΑ :

ΗΜΕΡΟΜΗΝΙΑ : ΜΑΪΟΣ 2018



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ΕΛΕΓΧΘΗΚΕ
ΟΙ ΕΠΙΒΛΕΠΟΝΤΕΣ

ΠΕΝΘΕΡΟΥΔΑΚΗΣ ΜΑΝΩΛΗΣ
Μηχανολόγος Μηχανικός

ΒΟΥΡΒΑΧΑΚΗΣ ΘΟΔΩΡΗΣ
Πολιτικός Μηχανικός

ΛΑΜΠΡΙΝΟΣ ΣΤΕΛΙΟΣ
Πολιτικός Μηχανικός

05-ΔΙΥΛΙΣΗ

Materials

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

No. 1 C 25/30 (EN 1992)

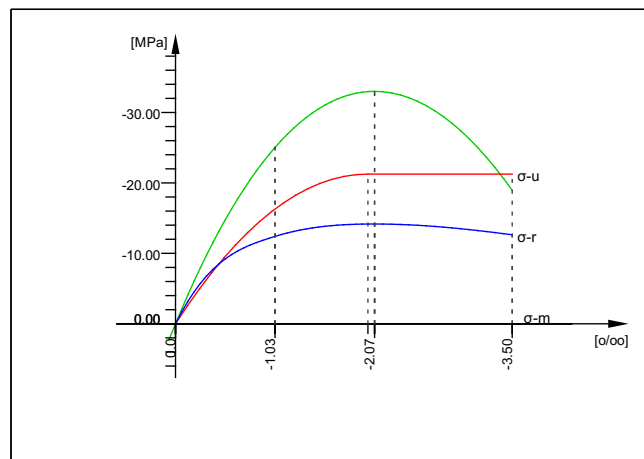
Young's modulus	E	15500	[N/mm ²]	Safetyfactor		1.50	[-]
Poisson ratio	μ	0.20	[-]	Strength	f _c	21.25	[MPa]
Shear modulus	G	6458	[N/mm ²]	Nominal strength	f _{ck}	25.00	[MPa]
Compression modulus	K	8611	[N/mm ²]	Tensile strength	f _{ctm}	2.56	[MPa]
Weight	γ	25.0	[kN/m ³]	Tensile strength	f _{ctk,05}	1.80	[MPa]
Density	ρ	2350.00	[kg/m ³]	Tensile strength	f _{ctk,95}	3.33	[MPa]
Elongation coefficient	α	1.00E-05	[1/K]	Bond strength	f _{bd}	2.69	[MPa]
				Service strength	f _{cm}	33.00	[MPa]
				Fatigue strength	f _{cd,fat}	15.00	[MPa]
				Tensile strength	f _{ctd}	1.20	[MPa]

Stress-Strain for serviceability	ε [o/oo]	σ-m [MPa]	E-t [N/mm ²]
Is also extended beyond the	0.000	0.00	33050
defined stress range	-1.035	-25.04	15658
	-2.069	-33.00	0
	-3.500	-18.95	-19203
	Safetyfactor		1.50

Stress-Strain for ultimate load	ε [o/oo]	σ-u [MPa]	E-t [N/mm ²]
Is only valid within the defined	0.000	0.00	21250
stress range	-2.000	-21.25	0
	-3.500	-21.25	0
	Safetyfactor		1.50

Stress-Strain of calc. mean values	ε [o/oo]	σ-r [MPa]	E-t [N/mm ²]
Is only valid within the defined	0.000	0.00	27541
stress range	-1.035	-12.41	4259
	-2.069	-14.17	0
	-3.500	-12.64	-1802
	Safetyfactor		(1.50)

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C 25/30 (EN 1992)

No. 2 B 500 C (EN 1992)

Young's modulus	E	200000	[N/mm ²]	Safetyfactor		1.15	[-]
Poisson ratio	μ	0.30	[-]	Yield stress	f _y	500.00	[MPa]
Shear modulus	G	76923	[N/mm ²]	Compressive yield	f _{yc}	500.00	[MPa]
Compression modulus	K	166667	[N/mm ²]	Tensile strength	f _t	575.00	[MPa]
Weight	γ	78.5	[kN/m ³]	Compressive strength	f _c	575.00	[MPa]
Density	ρ	7850.00	[kg/m ³]	Ultimate strain		75.00	[o/oo]
Elongation coefficient	α	1.20E-05	[1/K]	relative bond coeff.		1.00	[-]
max. thickness		32.00	[mm]	EN 1992 bond coeff.	k ₁	0.80	[-]
				Hardening modulus	E _h	0.00	[MPa]
				Proportional limit	f _p	500.00	[MPa]
				Dynamic allowance	σ-dyn	152.17	[MPa]

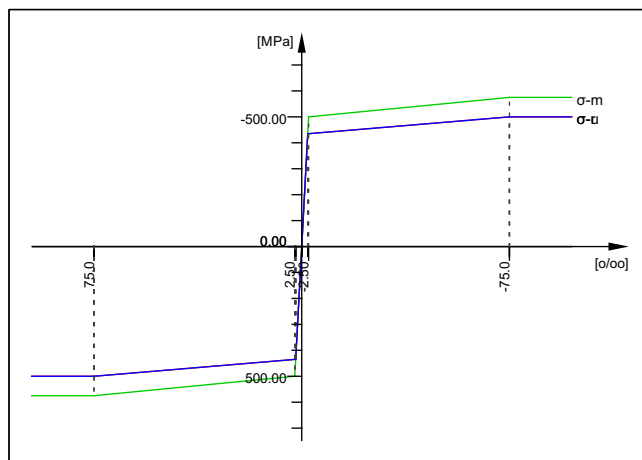
05-ΔΙΥΛΙΣΗ
 Materials

Stress-Strain for serviceability	ϵ [o/oo]	σ -m [MPa]	E-t [N/mm2]
Is also extended beyond the defined stress range	1000.000	575.00	0
	75.000	575.00	0
	2.500	500.00	1034
	0.000	0.00	200000
	-2.500	-500.00	1034
	-75.000	-575.00	0
	-1000.000	-575.00	0
Safetyfactor			1.15

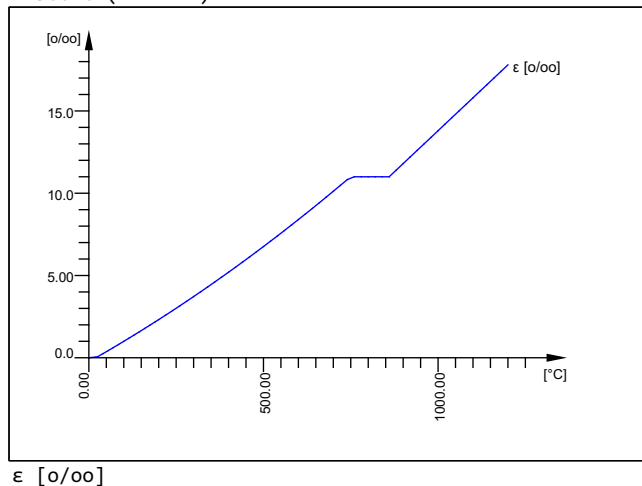
Stress-Strain for ultimate load	ϵ [o/oo]	σ -u [MPa]	E-t [N/mm2]
Is also extended beyond the defined stress range	1000.000	500.00	0
	75.000	500.00	0
	2.174	434.78	896
	0.000	0.00	200000
	-2.174	-434.78	896
	-75.000	-500.00	0
	-1000.000	-500.00	0
Safetyfactor			(1.15)

Stress-Strain of calc. mean values	ϵ [o/oo]	σ -r [MPa]	E-t [N/mm2]
Is also extended beyond the defined stress range	1000.000	500.00	0
	75.000	500.00	0
	2.174	434.78	896
	0.000	0.00	200000
	-2.174	-434.78	896
	-75.000	-500.00	0
	-1000.000	-500.00	0
Safetyfactor			(1.15)

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B 500 C (EN 1992)



No. 3 C 20/25 (EN 1992)

Young's modulus	E	29962	[N/mm2]	Safetyfactor		1.50	[-]
Poisson ratio	μ	0.20	[-]	Strength	f_c	20.00	[MPa]

05-ΔΙΥΛΙΣΗ
 Materials

No. 3 C 20/25 (EN 1992)

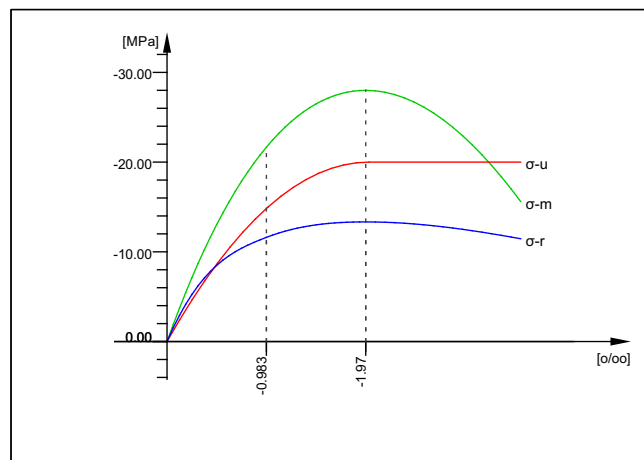
Shear modulus	G	12484	[N/mm ²]	Nominal strength	fck	20.00	[MPa]
Compression modulus	K	16646	[N/mm ²]	Tensile strength	fctm	2.21	[MPa]
Weight	γ	25.0	[kN/m ³]	Tensile strength	fctk,05	1.55	[MPa]
Density	ρ	2350.00	[kg/m ³]	Tensile strength	fctk,95	2.87	[MPa]
Elongation coefficient	α	1.00E-05	[1/K]	Bond strength	fbd	2.32	[MPa]
				Service strength	fcm	28.00	[MPa]
				Fatigue strength	fcd,fat	12.27	[MPa]
				Tensile strength	fctd	1.03	[MPa]

Stress-Strain for serviceability	ε [o/oo]	σ-m [MPa]	E-t [N/mm ²]
Is only valid within the defined stress range	0.000	0.00	31460
	-0.983	-21.66	13498
	-1.967	-28.00	0
	-3.500	-15.60	-15208
Safetyfactor			1.50

Stress-Strain for ultimate load	ε [o/oo]	σ-u [MPa]	E-t [N/mm ²]
Is only valid within the defined stress range	0.000	0.00	20000
	-2.000	-20.00	0
	-3.500	-20.00	0
Safetyfactor			1.50

Stress-Strain of calc. mean values	ε [o/oo]	σ-r [MPa]	E-t [N/mm ²]
Is only valid within the defined stress range	0.000	0.00	26217
	-0.983	-11.61	4353
	-1.967	-13.33	0
	-3.500	-11.46	-2034
Safetyfactor			(1.50)

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C 20/25 (EN 1992)

No. 4 C 30/37 (EN 1992)

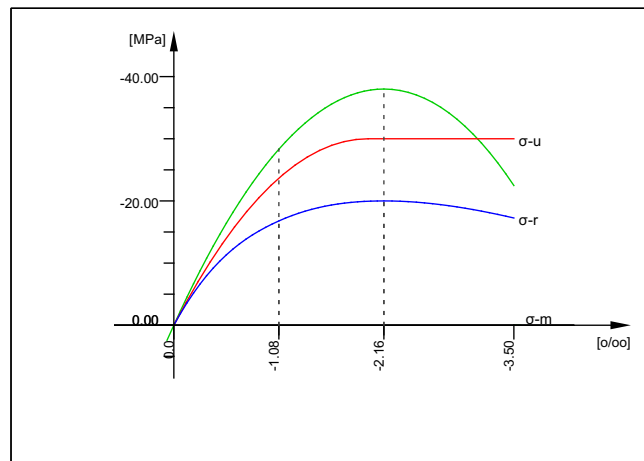
Young's modulus	E	16000	[N/mm ²]	Safetyfactor		1.50	[-]
Poisson ratio	μ	0.20	[-]	Strength	fc	30.00	[MPa]
Shear modulus	G	6667	[N/mm ²]	Nominal strength	fck	30.00	[MPa]
Compression modulus	K	8889	[N/mm ²]	Tensile strength	fctm	2.90	[MPa]
Weight	γ	25.0	[kN/m ³]	Tensile strength	fctk,05	2.03	[MPa]
Density	ρ	2350.00	[kg/m ³]	Tensile strength	fctk,95	3.77	[MPa]
Elongation coefficient	α	1.00E-05	[1/K]	Bond strength	fbd	3.04	[MPa]
				Service strength	fcm	38.00	[MPa]
				Fatigue strength	fcd,fat	17.60	[MPa]
				Tensile strength	fctd	1.35	[MPa]

Stress-Strain for serviceability	ε [o/oo]	σ-m [MPa]	E-t [N/mm ²]
Is also extended beyond the defined stress range	0.000	0.00	34478
	-1.081	-28.31	17746
	-2.162	-38.00	0
	-3.500	-22.47	-23499
Safetyfactor			1.50

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 Materials

Stress-Strain for ultimate load	ϵ [o/oo]	σ -u [MPa]	E-t [N/mm2]
Is only valid within the defined stress range	0.000	0.00	30000
	-2.000	-30.00	0
	-3.500	-30.00	0
Safetyfactor			1.50

Stress-Strain of calc. mean values	ϵ [o/oo]	σ -r [MPa]	E-t [N/mm2]
Is only valid within the defined stress range	0.000	0.00	28732
	-1.081	-16.78	7018
	-2.162	-20.00	0
	-3.500	-17.25	-3601
Safetyfactor			(1.50)



C 30/37 (EN 1992)

No. 5 C 25/30 (EN 1992) DUMMY

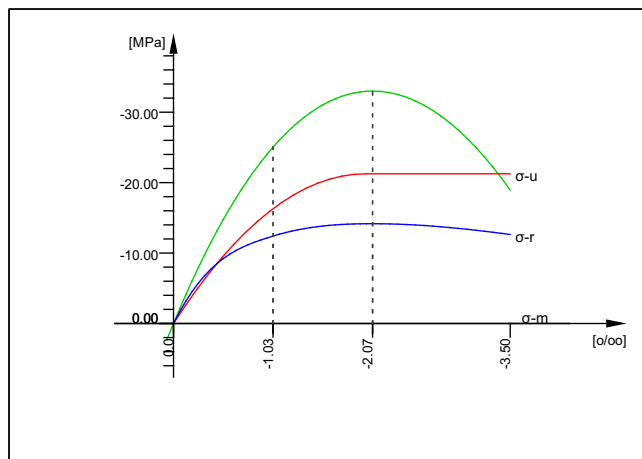
Young's modulus	E	1550000	[N/mm2]	Safetyfactor	1.50	[-]
Poisson ratio	μ	0.20	[-]	Strength	fc	21.25 [MPa]
Shear modulus	G	645833	[N/mm2]	Nominal strength	fck	25.00 [MPa]
Compression modulus	K	861111	[N/mm2]	Tensile strength	fctm	2.56 [MPa]
Weight	γ	25.0	[kN/m3]	Tensile strength	fctk,05	1.80 [MPa]
Density	ρ	2350.00	[kg/m3]	Tensile strength	fctk,95	3.33 [MPa]
Elongation coefficient	α	1.00E-07	[1/K]	Bond strength	fbd	2.69 [MPa]
				Service strength	fcm	33.00 [MPa]
				Fatigue strength	fcd,fat	15.00 [MPa]
				Tensile strength	fctd	1.20 [MPa]

Stress-Strain for serviceability	ϵ [o/oo]	σ -m [MPa]	E-t [N/mm2]
Is also extended beyond the defined stress range	0.000	0.00	33050
	-1.035	-25.04	15658
	-2.069	-33.00	0
	-3.500	-18.95	-19203
Safetyfactor			1.50

Stress-Strain for ultimate load	ϵ [o/oo]	σ -u [MPa]	E-t [N/mm2]
Is only valid within the defined stress range	0.000	0.00	21250
	-2.000	-21.25	0
	-3.500	-21.25	0
Safetyfactor			1.50

Stress-Strain of calc. mean values	ϵ [o/oo]	σ -r [MPa]	E-t [N/mm2]
Is only valid within the defined stress range	0.000	0.00	27541
	-1.035	-12.41	4259
	-2.069	-14.17	0
	-3.500	-12.64	-1802
Safetyfactor			(1.50)

05-ΔΙΥΛΙΣΗ
Materials



C 25/30 (EN 1992)DUMMY

05-ΔΙΥΛΙΣΗ

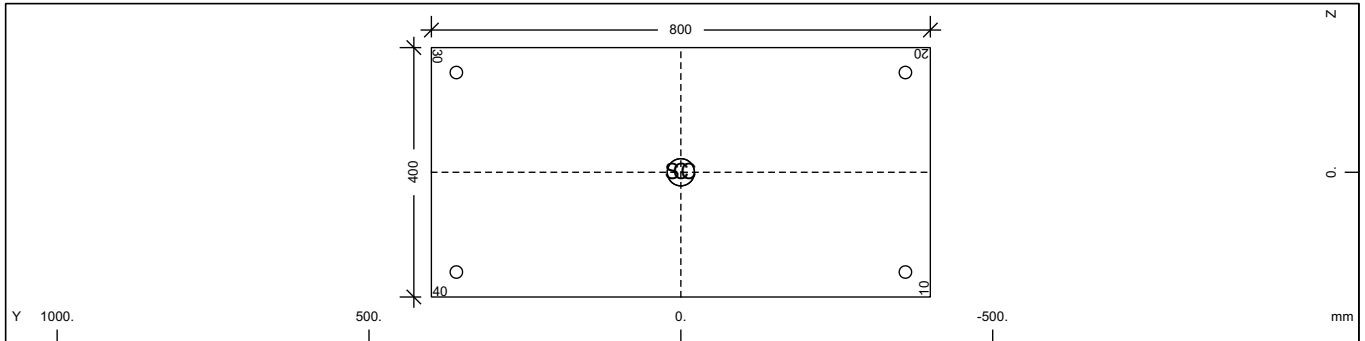
Sections

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992) DUMMY

Cross section No. 1 - B/H = 800 / 400 mm



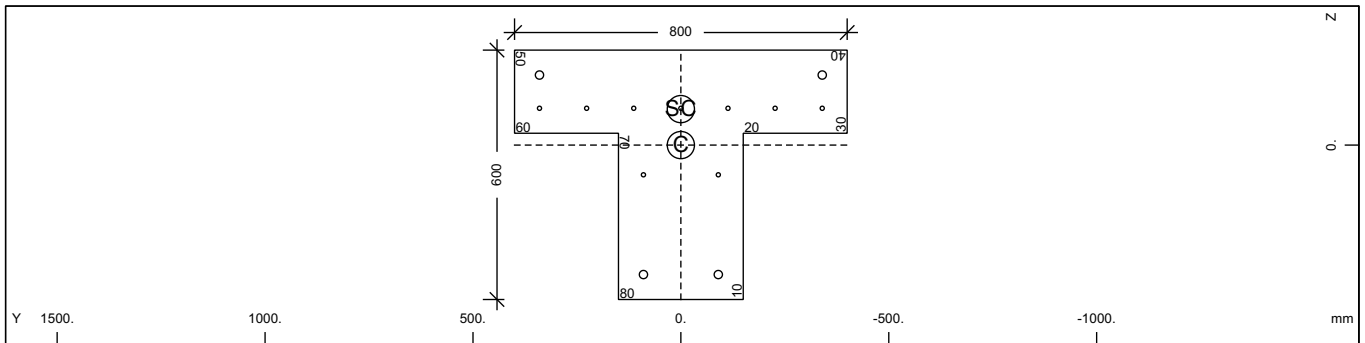
Cross section No. 1 - B/H = 800 / 400 mm

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
		It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
		Ayz[m2]	Iyz[m4]					
1	4	3.2000E-01		4.267E-03	0.0	0.0	16000	8.00
	2	1.172E-02		1.707E-02	0.0	0.0	6667	(COMPR)
		= B/H = 800 / 400 mm						
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

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Cross section No. 2 - B/H/Bw/Hf 800/600/300/200 mm



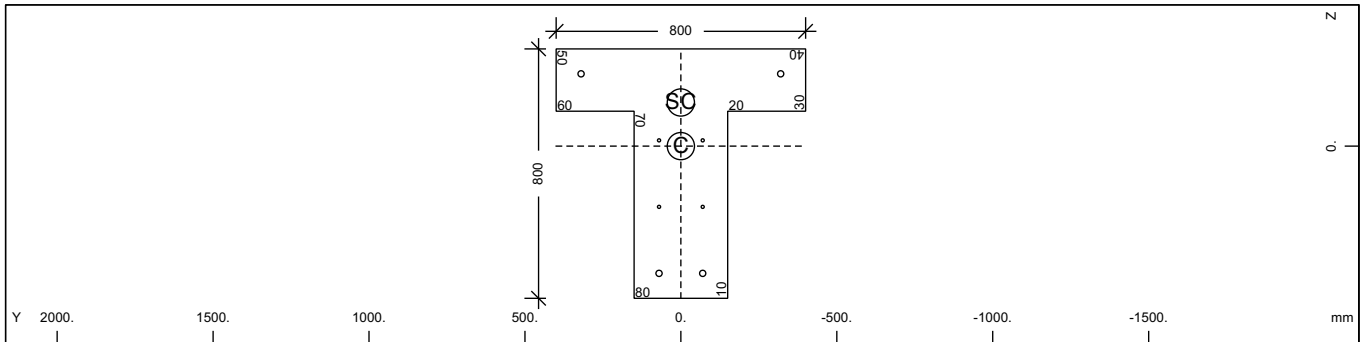
Cross section No. 2 - B/H/Bw/Hf 800/600/300/200 mm

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
		It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
		Ayz[m2]	Iyz[m4]					
2	4	2.8000E-01		8.305E-03	0.0	0.0	16000	7.00
	2	4.394E-04		9.433E-03	0.0	-86.7	6667	(CENTR)
		= B/H/Bw/Hf 800/600/300/200 mm						
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

05-ΔΙΥΛΙΣΗ
 Sections

Cross section No. 3 - B/H/Bw/Hf 800/800/300/200 mm

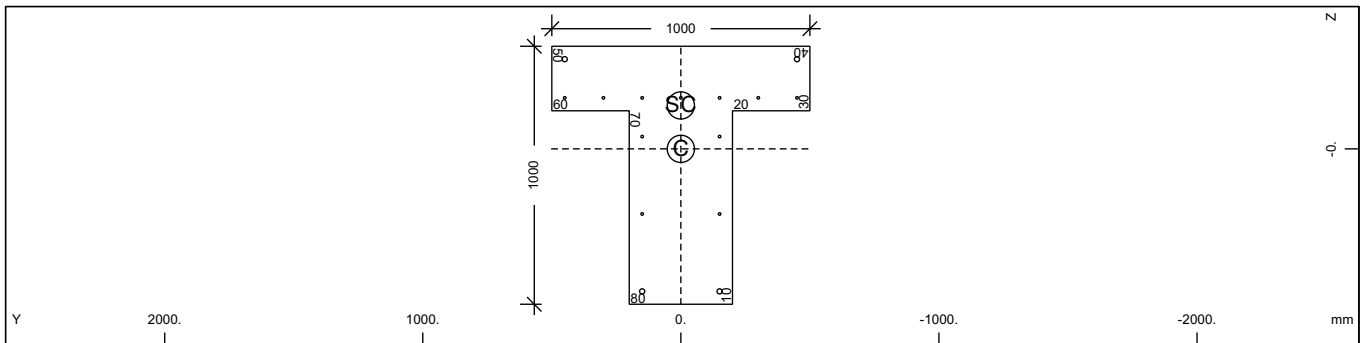


Cross section No. 3 - B/H/Bw/Hf 800/800/300/200 mm

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
	MRf	It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
			Ayz[m2]	Iyz[m4]				
3	4	3.4000E-01		1.949E-02	0.0	0.0	16000	8.50
	2	6.120E-04		9.883E-03	0.0	-139.8	6667	(CENTR)
= B/H/Bw/Hf 800/800/300/200 mm								
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

Cross section No. 4 - B/H/Bw/Hf 1000/1000/400/250 mm

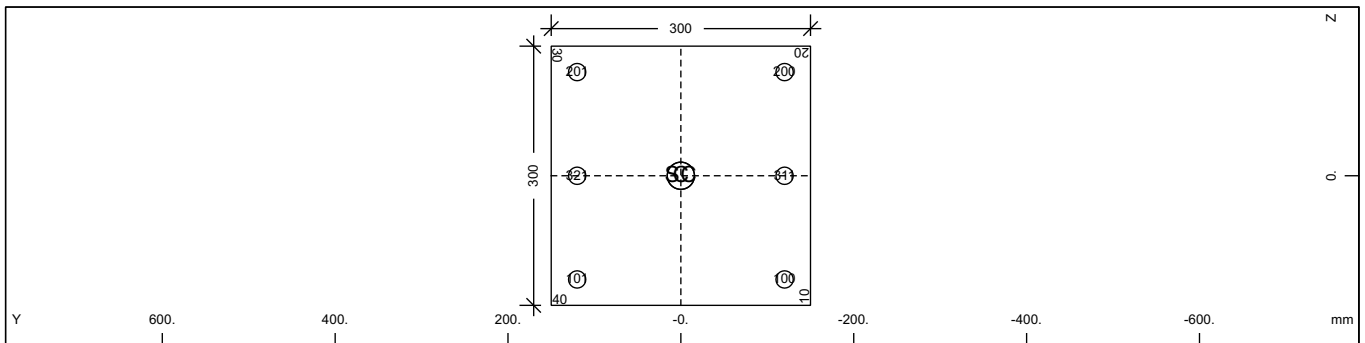


Cross section No. 4 - B/H/Bw/Hf 1000/1000/400/250 mm

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
	MRf	It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
			Ayz[m2]	Iyz[m4]				
4	4	5.5000E-01		4.946E-02	0.0	0.0	16000	13.75
	2	1.729E-03		2.483E-02	0.0	-168.3	6667	(CENTR)
= B/H/Bw/Hf 1000/1000/400/250 mm								
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

Cross section No. 25 - B/H = 300 / 300 mm



Cross section No. 25 - B/H = 300 / 300 mm

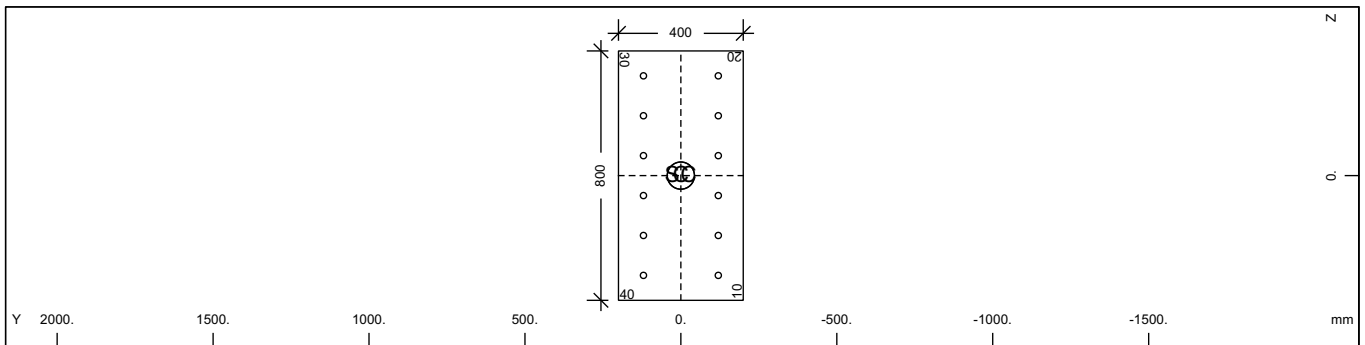
05-ΔΙΥΛΙΣΗ

Sections

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
		It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
		Ayz[m2]	Iyz[m4]					
25	4	9.0000E-02		6.750E-04	0.0	0.0	16000	2.25
	2	1.134E-03		6.750E-04	0.0	0.0	6667	
= B/H = 300 / 300 mm								
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

Cross section No. 101 - B/H = 400 / 800 mm



Cross section No. 101 - B/H = 400 / 800 mm

Static properties of cross section

No.	Mat	A[m2]	Ay[m2]	Iy[m4]	yc[mm]	ysc[mm]	E[N/mm2]	g[kN/m]
		It[m4]	Az[m2]	Iz[m4]	zc[mm]	zsc[mm]	G[N/mm2]	
		Ayz[m2]	Iyz[m4]					
101	4	3.2000E-01		1.707E-02	0.0	0.0	16000	8.00
	2	1.172E-02		4.267E-03	0.0	0.0	6667	
= B/H = 400 / 800 mm								
No.	section number			ysc,zsc	shear centre			
Mat	material number			E	Young's modulus			
A	sectional area			g	weight per length			
Ay,Az,Ayz	transverse shear deformation area			MRf	reinforcement material number			
Iy,Iz,Iyz	bending moment of inertia			It	torsional moment of inertia			
yc,zc	centre of gravity			G	Shear modulus			

KGS AIRPORT - MODULE M02 - REV 01
 Generation of Node and Element Loads

Actions

type	part	sup	Title	$\gamma-u$	$\gamma-f$	$\gamma-a$	$\psi-0$	$\psi-1$	$\psi-2$	$\psi-1'$
G	G	perm	dead load	1.35	1.00	1.00	1.00	1.00	1.00	1.00
			1 SW							
			2 SDL							
			4 SH (-15)							
			6 EARTH PRESSURE							
			8 YDROSTATIKH							
Q	Q	cond	variable load	1.50	0.00	1.00	0.70	0.50	0.30	1.00
			3 LL							
			5 TEMP(-20)							
			Reduction coefficient	xsi	0.850					

Load Case 1 (G) SW

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.000
 Factor dead weight DL-YY 0.000
 Factor dead weight DL-ZZ -1.000
 unfavourable safety factor 1.350
 favourable safety factor 1.000
 Combination coefficient $\psi-0$ 1.000 (rare)
 Combination coefficient $\psi-1'$ 1.000 (non frequent)
 Combination coefficient $\psi-1$ 1.000 (frequent)
 Combination coefficient $\psi-2$ 1.000 (permanent)

Load Case 2 (G) SDL

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.000
 Factor dead weight DL-YY 0.000
 Factor dead weight DL-ZZ 0.000
 unfavourable safety factor 1.350
 favourable safety factor 1.000
 Combination coefficient $\psi-0$ 1.000 (rare)
 Combination coefficient $\psi-1'$ 1.000 (non frequent)
 Combination coefficient $\psi-1$ 1.000 (frequent)
 Combination coefficient $\psi-2$ 1.000 (permanent)

Load Case 3 (Q) LL

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.000
 Factor dead weight DL-YY 0.000
 Factor dead weight DL-ZZ 0.000
 unfavourable safety factor 1.500
 favourable safety factor 0.000
 Combination coefficient $\psi-0$ 0.700 (rare)
 Combination coefficient $\psi-1'$ 1.000 (non frequent)
 Combination coefficient $\psi-1$ 0.500 (frequent)
 Combination coefficient $\psi-2$ 0.300 (permanent)

Load Case 4 (G) SH (-15)

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.000
 Factor dead weight DL-YY 0.000
 Factor dead weight DL-ZZ 0.000
 unfavourable safety factor 1.350
 favourable safety factor 1.000
 Combination coefficient $\psi-0$ 1.000 (rare)
 Combination coefficient $\psi-1'$ 1.000 (non frequent)
 Combination coefficient $\psi-1$ 1.000 (frequent)
 Combination coefficient $\psi-2$ 1.000 (permanent)

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Generation of Node and Element Loads

Load Case 5 (Q) TEMP(-20)

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	0.000
unfavourable safety factor		1.500
favourable safety factor		0.000
Combination coefficient $\psi-0$		0.700 (rare)
Combination coefficient $\psi-1'$		1.000 (non frequent)
Combination coefficient $\psi-1$		0.500 (frequent)
Combination coefficient $\psi-2$		0.300 (permanent)

Load Case 6 (G) EARTH PRESSURE

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	0.000
unfavourable safety factor		1.350
favourable safety factor		1.000
Combination coefficient $\psi-0$		1.000 (rare)
Combination coefficient $\psi-1'$		1.000 (non frequent)
Combination coefficient $\psi-1$		1.000 (frequent)
Combination coefficient $\psi-2$		1.000 (permanent)

Load Case 8 (G) YDROSTATIKH

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	0.000
unfavourable safety factor		1.350
favourable safety factor		1.000
Combination coefficient $\psi-0$		1.000 (rare)
Combination coefficient $\psi-1'$		1.000 (non frequent)
Combination coefficient $\psi-1$		1.000 (frequent)
Combination coefficient $\psi-2$		1.000 (permanent)

05-ΔΙΥΛΙΣΗ

Calculation of forces and moments

Load Case 1 (G) SW

Factor forces and moments	1.000
Factor dead weight DL-ZZ	-1.000
unfavourable safety factor	1.350
favourable safety factor	1.000
Combination coefficient $\psi-0$	1.000 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	1.000 (frequent)
Combination coefficient $\psi-2$	1.000 (permanent)

Load Case 2 (G) SDL

Factor forces and moments	1.000
unfavourable safety factor	1.350
favourable safety factor	1.000
Combination coefficient $\psi-0$	1.000 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	1.000 (frequent)
Combination coefficient $\psi-2$	1.000 (permanent)

Load Case 3 (Q) LL

Factor forces and moments	1.000
unfavourable safety factor	1.500
favourable safety factor	0.000
Combination coefficient $\psi-0$	0.700 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	0.500 (frequent)
Combination coefficient $\psi-2$	0.300 (permanent)

Load Case 4 (G) SH (-15)

Factor forces and moments	1.000
unfavourable safety factor	1.350
favourable safety factor	1.000
Combination coefficient $\psi-0$	1.000 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	1.000 (frequent)
Combination coefficient $\psi-2$	1.000 (permanent)

Load Case 5 (Q) TEMP(-20)

Factor forces and moments	1.000
unfavourable safety factor	1.500
favourable safety factor	0.000
Combination coefficient $\psi-0$	0.700 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	0.500 (frequent)
Combination coefficient $\psi-2$	0.300 (permanent)

Load Case 6 (G) EARTH PRESSURE

Factor forces and moments	1.000
unfavourable safety factor	1.350
favourable safety factor	1.000
Combination coefficient $\psi-0$	1.000 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	1.000 (frequent)
Combination coefficient $\psi-2$	1.000 (permanent)

Load Case 8 (G) YDROSTATIKH

Factor forces and moments	1.000
unfavourable safety factor	1.350
favourable safety factor	1.000
Combination coefficient $\psi-0$	1.000 (rare)
Combination coefficient $\psi-1'$	1.000 (non frequent)
Combination coefficient $\psi-1$	1.000 (frequent)
Combination coefficient $\psi-2$	1.000 (permanent)

05-ΔΙΥΛΙΣΗ

Calculation of forces and moments

Load Case 201 EQ_Y-Y q=1.50

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.138
 Factor dead weight DL-YY 0.460
 Factor dead weight DL-ZZ -1.000
 Loads partially copied from load case 2 with factor 1.000
 Loads partially copied from load case 3 with factor 0.300

Load Case 202 EQ_X-X q=1.50

Factor forces and moments 1.000
 Factor dead weight DL-XX 0.460
 Factor dead weight DL-YY 0.138
 Factor dead weight DL-ZZ -1.000
 Loads partially copied from load case 2 with factor 1.000
 Loads partially copied from load case 3 with factor 0.300

Sum of Loadings

Loadcase	Σ(Loads)			Title
	X[kN]	Y[kN]	Z[kN]	
1	0.0	0.0	-41095.9	SW
2	0.0	0.0	-4308.5	SDL
3	0.0	0.0	-7180.8	LL
4	0.0	0.0	0.0	SH (-15)
5	0.0	0.0	0.0	TEMP(-20)
6	-0.0	0.8	0.0	EARTH PRESSURE
8	-1531.4	-0.7	-48413.0	YDROSTATIKH
201	6486.7	21622.3	-47558.7	EQ_Y-Y q=1.50
202	21622.3	6486.7	-47558.7	EQ_X-X q=1.50

05-ΔΙΥΛΙΣΗ

Actions

type	part	sup	Title	$\gamma-u$	$\gamma-f$	$\gamma-a$	$\psi-0$	$\psi-1$	$\psi-2$	$\psi-1'$
G	G	perm	dead load	1.35	1.00	1.00	1.00	1.00	1.00	1.00
Q	Q	cond	variable load	1.50	0.00	1.00	0.70	0.50	0.30	1.00
			Reduction coefficient		xsi	0.850				

Load Case 201 EQ_Y-Y q=3.00

Factor forces and moments	1.000
Factor dead weight DL-XX	0.069
Factor dead weight DL-YY	0.230
Factor dead weight DL-ZZ	-1.000
Loads partially copied from load case 2 with factor	1.000
Loads partially copied from load case 3 with factor	0.300

05-ΔΙΥΛΙΣΗ

Load Case 201 EQ_Y-Y q=3.00

Factor forces and moments 1.000
Factor dead weight DL-XX 0.069
Factor dead weight DL-YY 0.230
Factor dead weight DL-ZZ -1.000
Loads partially copied from load case 2 with factor 1.000
Loads partially copied from load case 3 with factor 0.300

Sum of Loadings

Loadcase	Σ(Loads)			Title
	X[kN]	Y[kN]	Z[kN]	
201	3243.4	10811.2	-47558.7	EQ_Y-Y q=3.00

05-ΔΙΥΛΙΣΗ

Load Case 202 EQ_Y-Y q=3.00

Factor forces and moments		1.000		
Factor dead weight	DL-XX	0.230		
Factor dead weight	DL-YY	0.069		
Factor dead weight	DL-ZZ	-1.000		
Loads partially copied from load case			2 with factor	1.000
Loads partially copied from load case			3 with factor	0.300

05-ΔΙΥΛΙΣΗ

Load Case 202 EQ_X-X q=3.00

Factor forces and moments 1.000
Factor dead weight DL-XX 0.230
Factor dead weight DL-YY 0.069
Factor dead weight DL-ZZ -1.000
Loads partially copied from load case 2 with factor 1.000
Loads partially copied from load case 3 with factor 0.300

Sum of Loadings

Loadcase	Σ(Loads)			Title
	X[kN]	Y[kN]	Z[kN]	
202	10811.2	3243.4	-47558.7	EQ_X-X q=3.00

05-ΔΙΥΛΙΣΗ

ULS COMBINATIONS NO EQ

Actions

type	part	sup	Title	$\gamma-u$	$\gamma-f$	$\gamma-a$	$\psi-0$	$\psi-1$	$\psi-2$	$\psi-1'$
G	G	perm	dead load	1.35	1.00	1.00	1.00	1.00	1.00	1.00
Q	Q	cond	variable load	1.50	0.00	1.00	0.70	0.50	0.30	1.00
			Reduction coefficient		xsi	0.850				

Load Case 101 ((D))

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	-1.350
Loads partially copied from load case	1 with factor	1.350
Loads partially copied from load case	2 with factor	1.350
Loads partially copied from load case	3 with factor	1.500
Loads partially copied from load case	6 with factor	1.350
Loads partially copied from load case	8 with factor	1.350

Load Case 102 ((D))

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	-1.350
Loads partially copied from load case	1 with factor	1.350
Loads partially copied from load case	2 with factor	1.350
Loads partially copied from load case	3 with factor	1.500
Loads partially copied from load case	4 with factor	1.000
Loads partially copied from load case	6 with factor	1.350
Loads partially copied from load case	8 with factor	1.350

Load Case 103 ((D))

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	-1.350
Loads partially copied from load case	1 with factor	1.350
Loads partially copied from load case	2 with factor	1.350
Loads partially copied from load case	3 with factor	1.500
Loads partially copied from load case	4 with factor	1.000
Loads partially copied from load case	5 with factor	0.900
Loads partially copied from load case	6 with factor	1.350
Loads partially copied from load case	8 with factor	1.350

Load Case 104 ((D))

Factor forces and moments		1.000
Factor dead weight	DL-XX	0.000
Factor dead weight	DL-YY	0.000
Factor dead weight	DL-ZZ	-1.350
Loads partially copied from load case	1 with factor	1.350
Loads partially copied from load case	2 with factor	1.350
Loads partially copied from load case	3 with factor	1.050
Loads partially copied from load case	4 with factor	1.000
Loads partially copied from load case	5 with factor	1.500
Loads partially copied from load case	6 with factor	1.350
Loads partially copied from load case	8 with factor	1.350

05-ΔΙΥΛΙΣΗ

ULS COMBINATIONS NO EQ (101-104)

Reduced Beam-Stiffness in a Slab

cno	d-slab [m]	b-slab [m]	IY-0 [m4]	IY-red [m4]	A-0 [m2]	A-red [m2]	G-0 [kN/m3]	G-red [kN/m3]
1	0.240	0.400	4.267E-03	3.820E-03	0.3200	0.2240	25.0	17.5
1	0.267	0.800	4.267E-03	3.042E-03	0.3200	0.1067	25.0	8.3
2	0.200	0.400	8.305E-03	8.046E-03	0.2800	0.2000	25.0	17.9
2	0.200	0.800	8.305E-03	7.788E-03	0.2800	0.1200	25.0	10.7
3	0.250	0.400	1.949E-02	1.898E-02	0.3400	0.2400	25.0	17.6
3	0.250	0.800	1.949E-02	1.848E-02	0.3400	0.1400	25.0	10.3
4	0.250	1.000	4.946E-02	4.819E-02	0.5500	0.3000	25.0	13.6
101	0.240	0.400	1.707E-02	1.662E-02	0.3200	0.2240	25.0	17.5

The following nodes have been detected to connect beams with wall elements. The adjacent quad elements will get an internal inplane torsional stiffness to transform the bending moment into pairs of forces on the quad nodes (see CTRL INPL):

1136 1139 1142 1144 1151 1160 1165 1166

++++ warning no. 125 in program QUAD
 Element 21228 edge too small -> WING-Extra-Elementinfo-QUADinfo
 +++++ warning no. 125 in program QUAD
 Element 21233 edge too small -> WING-Extra-Elementinfo-QUADinfo
 +++++ warning no. 125 in program QUAD
 Element 32000 edge too small -> WING-Extra-Elementinfo-QUADinfo
 +++++ warning no. 125 in program QUAD
 Element 32003 edge too small -> WING-Extra-Elementinfo-QUADinfo
 +++++ warning no. 125 in program QUAD
 Element 32020 edge too small -> WING-Extra-Elementinfo-QUADinfo
 +++++ warning no. 125 in program QUAD
 Element 32021 edge too small -> WING-Extra-Elementinfo-QUADinfo

Load Case 101 ((D))

Factor forces and moments 1.000
 Factor dead weight DL-ZZ -1.350
 Loads partially copied from load case 1 with factor 1.350
 Loads partially copied from load case 2 with factor 1.350
 Loads partially copied from load case 3 with factor 1.500
 Loads partially copied from load case 6 with factor 1.350
 Loads partially copied from load case 8 with factor 1.350

Sum of Loadings

Loadcase	Σ(Loads)			Title
	X[kN]	Y[kN]	Z[kN]	
101	-2067.5	0.1	-137424.8	

Sum of Reactions and Loadings

Loadcase	Σ(Reactions)			Title
	X[kN]	Y[kN]	Z[kN]	
	Σ(Loads)			
101	2067.5	-0.1	137424.7	DLZ= -1.35 sum_PZ=-137.4 MN .
	-2067.5	0.1	-137424.3	

05-ΔΙΥΛΙΣΗ

ULS COMBINATIONS NO EQ (101-104)

Load Case 102 ((D))

Factor forces and moments	1.000		
Factor dead weight	DL-ZZ	-1.350	
Loads partially copied from load case	1 with factor	1.350	
Loads partially copied from load case	2 with factor	1.350	
Loads partially copied from load case	3 with factor	1.500	
Loads partially copied from load case	4 with factor	1.000	
Loads partially copied from load case	6 with factor	1.350	
Loads partially copied from load case	8 with factor	1.350	

05-ΔΙΥΛΙΣΗ

ULS COMBINATIONS NO EQ (101-104)

Analysis parameters

Calculation with nonlinear material properties

Nonlinear material properties are used for:

Springelements[CRAC,YIEL,MUE,GAP], pilebedding, QUAD-bedding

Only linear material properties are used for:

QUAD- and BRIQ-elements

Truss-, cable-, Beam-, pile- und boundaryelements

Beamelements

++++ warning no. 270 in program STAB
T-beam components: E*A-slab > 0.9*E*A-beam for beam 10034 >echo plab extr
++++ warning no. 271 in program STAB
T-beam components - IY-slab greater than 0.8*IY-beam for beam 10034
++++ warning no. 270 in program STAB
T-beam components: E*A-slab > 0.9*E*A-beam for beam 10035 >echo plab extr
++++ warning no. 271 in program STAB
T-beam components - IY-slab greater than 0.8*IY-beam for beam 10035
++++ warning no. 270 in program STAB
T-beam components: E*A-slab > 0.9*E*A-beam for beam 10036 >echo plab extr
++++ warning no. 271 in program STAB
T-beam components - IY-slab greater than 0.8*IY-beam for beam 10036
++++ warning no. 270 in program STAB
T-beam components: E*A-slab > 0.9*E*A-beam for beam 10037 >echo plab extr
++++ warning no. 271 in program STAB
T-beam components - IY-slab greater than 0.8*IY-beam for beam 10037
++++ warning no. 270 in program STAB
T-beam components: E*A-slab > 0.9*E*A-beam for beam 10053 >echo plab extr
++++ warning no. 271 in program STAB
T-beam components - IY-slab greater than 0.8*IY-beam for beam 10053
++++ warning no. 129 in program STAB
Further warnings of type no 270 are suppressed
++++ warning no. 129 in program STAB
Further warnings of type no 271 are suppressed
++++ warning no. 267 in program STAB
FE-slabthicknes not equal T-beam-slabthicknes for cross section 3

Load Case 103 ((D))

Factor forces and moments	1.000
Factor dead weight	DL-ZZ -1.350
Loads partially copied from load case	1 with factor 1.350
Loads partially copied from load case	2 with factor 1.350
Loads partially copied from load case	3 with factor 1.500
Loads partially copied from load case	4 with factor 1.000
Loads partially copied from load case	5 with factor 0.900
Loads partially copied from load case	6 with factor 1.350
Loads partially copied from load case	8 with factor 1.350

05-ΔΙΥΛΙΣΗ

ULS COMBINATIONS NO EQ (101-104)

Load Case 104 ((D))

Factor forces and moments 1.000
Factor dead weight DL-ZZ -1.350
Loads partially copied from load case 1 with factor 1.350
Loads partially copied from load case 2 with factor 1.350
Loads partially copied from load case 3 with factor 1.050
Loads partially copied from load case 4 with factor 1.000
Loads partially copied from load case 5 with factor 1.500
Loads partially copied from load case 6 with factor 1.350
Loads partially copied from load case 8 with factor 1.350

Sum of Loadings

Loadcase	Σ(Loads)			Title
	X[kN]	Y[kN]	Z[kN]	
104	-2067.5	0.1	-134193.4	

05-ΔΙΥΛΙΣΗ

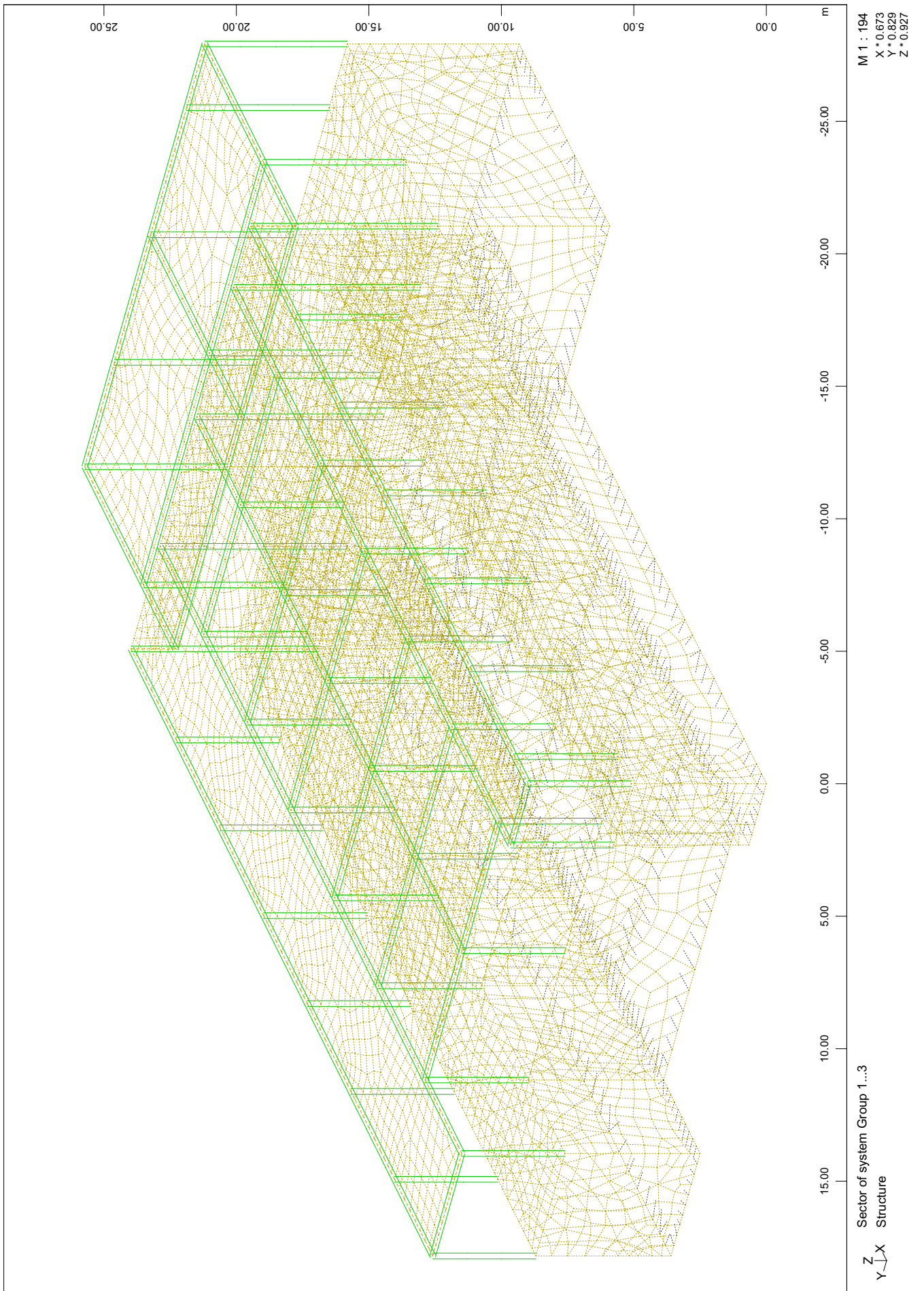
SLS COMBINATIONS (301)

Load Case 301 ((P))

Factor forces and moments			1.000
Factor dead weight	DL-ZZ		-1.000
Loads partially copied from load case	1 with factor		1.000
Loads partially copied from load case	2 with factor		1.000
Loads partially copied from load case	3 with factor		1.000
Loads partially copied from load case	4 with factor		1.000
Loads partially copied from load case	5 with factor		1.000
Loads partially copied from load case	6 with factor		1.000
Loads partially copied from load case	8 with factor		1.000

05-ΔΙΥΛΙΣΗ
ΠΡΟΣΟΜΟΙΩΜΑ ΥΠΟΛΟΓΙΣΜΟΥ/CALCULATION MODEL

SOFISTIK AG - www.sofistik.de



05-ΔΙΥΛΙΣΗ

ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS

```
1 PROG WING $ Interactive Graphics
2 $ Dat : C:\...\sk\05-DIYLISH-PD-R0\SOFI\DIYLISH.dat (#00h)          6/17/2018
3 $ Job : 000520                                                    1:31
4 HEAD $All loads LC:      2
5 PAGE UNII 0
6 CTRL OPT INP
7 CTRL OPT GSTR VAL DEFA
8 CTRL OPT AXIS VAL DEFA
9 $ graphics 1 | Picture 1 | Layer 1 : All loads LC:      2
10 PAGE LANO 1 UNIO 5
11 SIZE TYPE URS SC 0 SPLI '1*1'
12 SIZ2 SPLI DEFA
13 HEAD ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS
14 AND POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
15 SCHH H6 0.230000
16 SCH2 DIRE DEFA
17 LC NO 2 DESI 1
18 MOVE X DEL DTYP QSEC
19 BOX
20 VIEW TYPE DIRE X 0 Y 0 Z -1 AXIS NEGY ROTA 0
21 DEFO TYPE NO EXPO 0 SMOV NO
22 SELE NUMB 0
23 MOVE X -1.605806 Y 33.76949 Z 0 UNIT WC A 0 SCHH 0.300000 FACW 0.700000 MARG 0 C 3001 CB 101 ALIG DEFA SET PBE
24 DRAW X 38.77285 Y 33.76949 Z 0 UNIT WC DTYP QSEC GRP NO MNO NO HINT NO DIST DEFA
25 MOVE X 5.492138 Y 40.01123 Z 0 UNIT WC GRNO 0 DTYP QSEC
26 DRAW X 5.492138 Y -1.848656 Z 0 UNIT WC DTYP QSEC
27 GRP NUMB NODE OPTI OFFL
28 GRP NUMB ENOD OPTI OFFL
29 GRP NUMB EDGE OPTI OFFL
30 GRP LC NO
31 GRP NUMB 0 YES GLN
32 GRP NUMB 0 YES QSEC
33 LOOP#GRP 2 ; GRP NUMB 1+#GRP YES BEAM,QUAD,GLN,GAR ; ENDL00P
34 GRP NUMB 3 OFF BEAM,GLN
35 GRP NUMB 3 YES QUAD,GAR
36 GRP NUMB 4 YES QUAD,GAR
37 GRP NUMB 5 OFF BEAM,GLN
38 GRP NUMB 5 YES QUAD,GAR
39 LOOP#GRP 3 ; GRP NUMB 10+#GRP YES QUAD,GAR ; ENDL00P
40 GRP NUMB 15 OFF
41 GRP NUMB 16 YES QUAD,GAR
42 GRP NUMB 20 OFF
43 GRP NUMB 101 OFF
44 GRP NUMB 103 OFF
45 GRP NUMB 105 OFF
46 GRP NUMB 115 OFF
47 GRP NUMB 300 OFF
48 GRP NUMB 400 OFF
49 VIEW TYPE DIRE X 0.739337 Y 0.558893 Z -0.375525 AXIS NEGZ ROTA 0
50 SELE NUMB 0
51 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
52 $ graphics 2 | Picture 1 | Layer 1 : All loads LC:      3
53 SIZ2
54 AND POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
55 LC NO 3
56 GRP NUMB 0 YES GLN
57 GRP NUMB 0 YES QSEC
58 LOOP#GRP 3 ; GRP NUMB 1+#GRP YES BEAM,QUAD,GLN,GAR ; ENDL00P
59 GRP NUMB 4 YES QUAD,GAR
60 GRP NUMB 5 YES BEAM,QUAD,GLN,GAR
61 LOOP#GRP 3 ; GRP NUMB 10+#GRP YES QUAD,GAR ; ENDL00P
62 GRP NUMB 15 YES BEAM,GLN
63 GRP NUMB 16 YES QUAD,GAR
64 GRP NUMB 20 OFF
65 GRP NUMB 101 YES BEAM,GLN
66 GRP NUMB 103 OFF BOUN
67 GRP NUMB 103 YES BEAM,GLN
68 GRP NUMB 105 YES BEAM,GLN
```

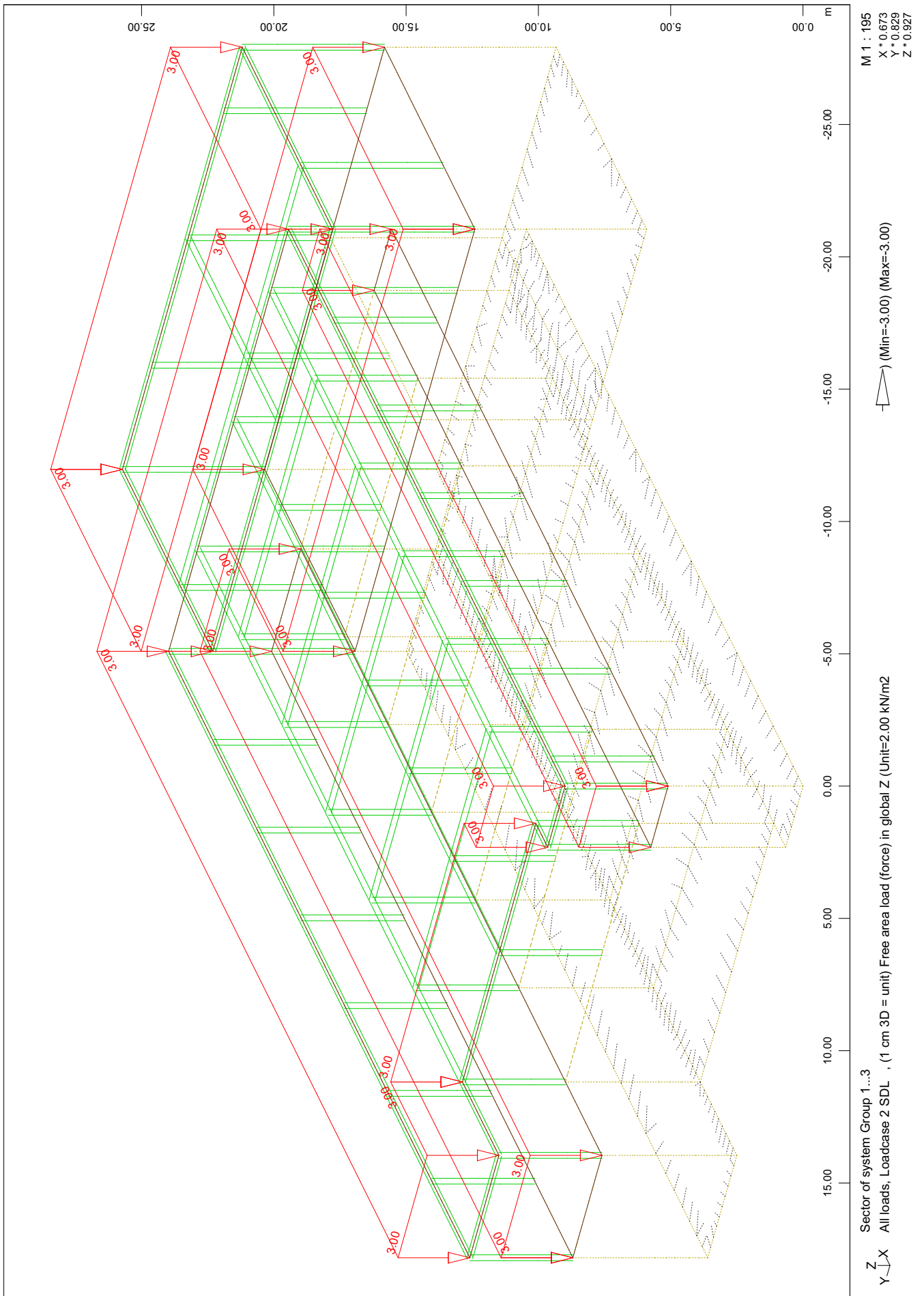
05-ΔΙΥΛΙΣΗ

ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS

```
69 GRP  NUMB 115 YES BEAM,GLN
70 GRP  NUMB 300 OFF
71 GRP  NUMB 400 YES BEAM,GLN
72 SELE NUMB 0
73 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
74 $ graphics 3 | Picture 1 | Layer 1 : All loads LC: 6
75 SIZ2
76 AND  POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
77 LC  NO 6
78 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
79 $ graphics 4 | Picture 1 | Layer 1 : All loads LC: 7
80 SIZ2
81 AND  POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
82 LC  NO 7
83 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
++++ warning no. 806 in program gr3_e_last
          LOAD TYPE ALL loadcase 7 not valid : No values found
84 $ graphics 5 | Picture 1 | Layer 1 : All loads LC: 8
85 SIZ2
86 AND  POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
87 LC  NO 8
88 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
89 $ graphics 6 | Picture 1 | Layer 1 : All loads LC: 9
90 SIZ2
91 AND  POSI 1 POSL 0 POSR 100 POSD 0 POSU 100
92 LC  NO 9
93 LOAD TYPE ALL UNIT DEFA SCHH YES SING VECT FILL NO REPR DREP ETYP ALL GTYP INP
++++ warning no. 806 in program gr3_e_last
          LOAD TYPE ALL loadcase 9 not valid : No values found
94 END
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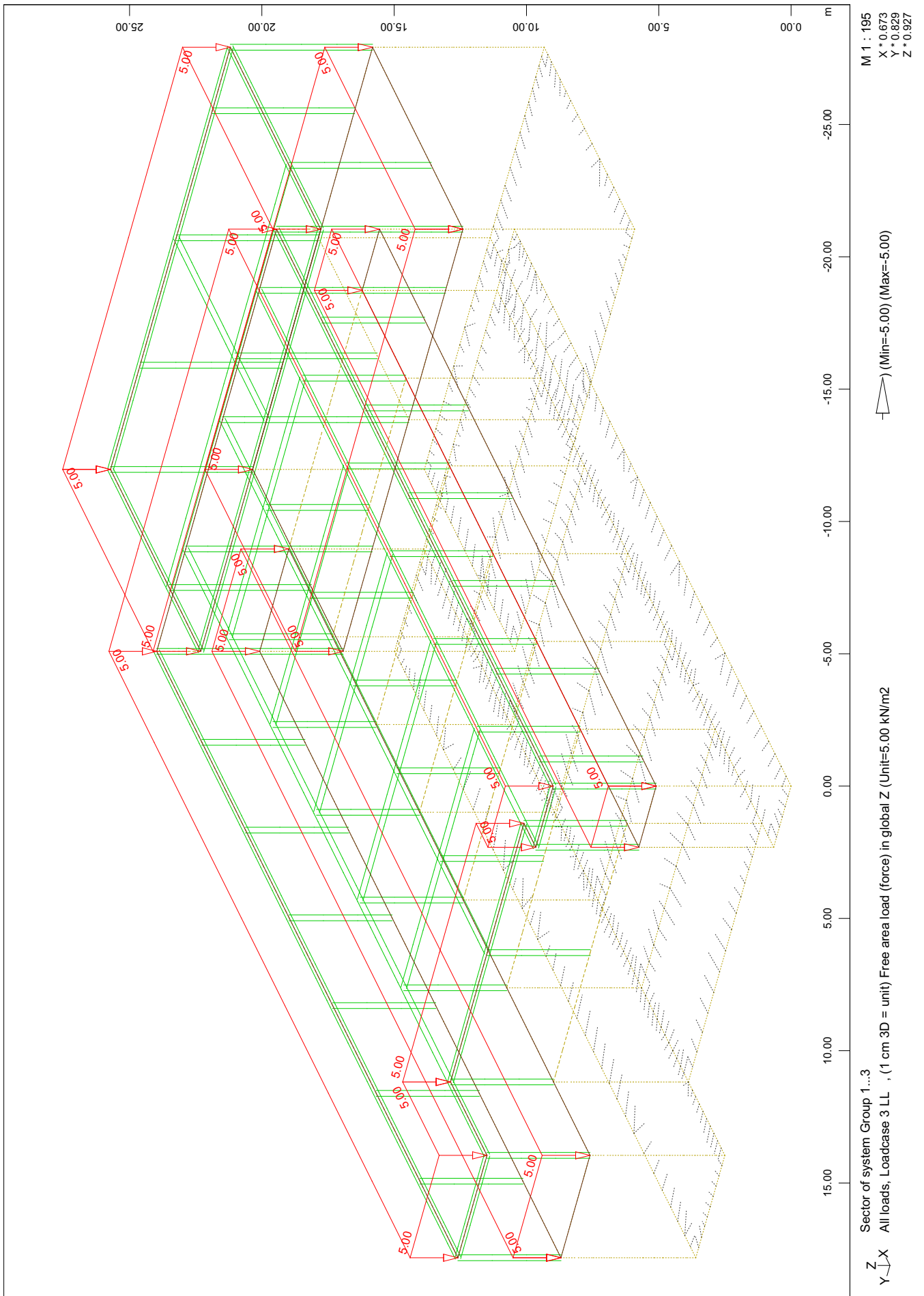
05-ΔΙΥΛΙΣΗ
ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS

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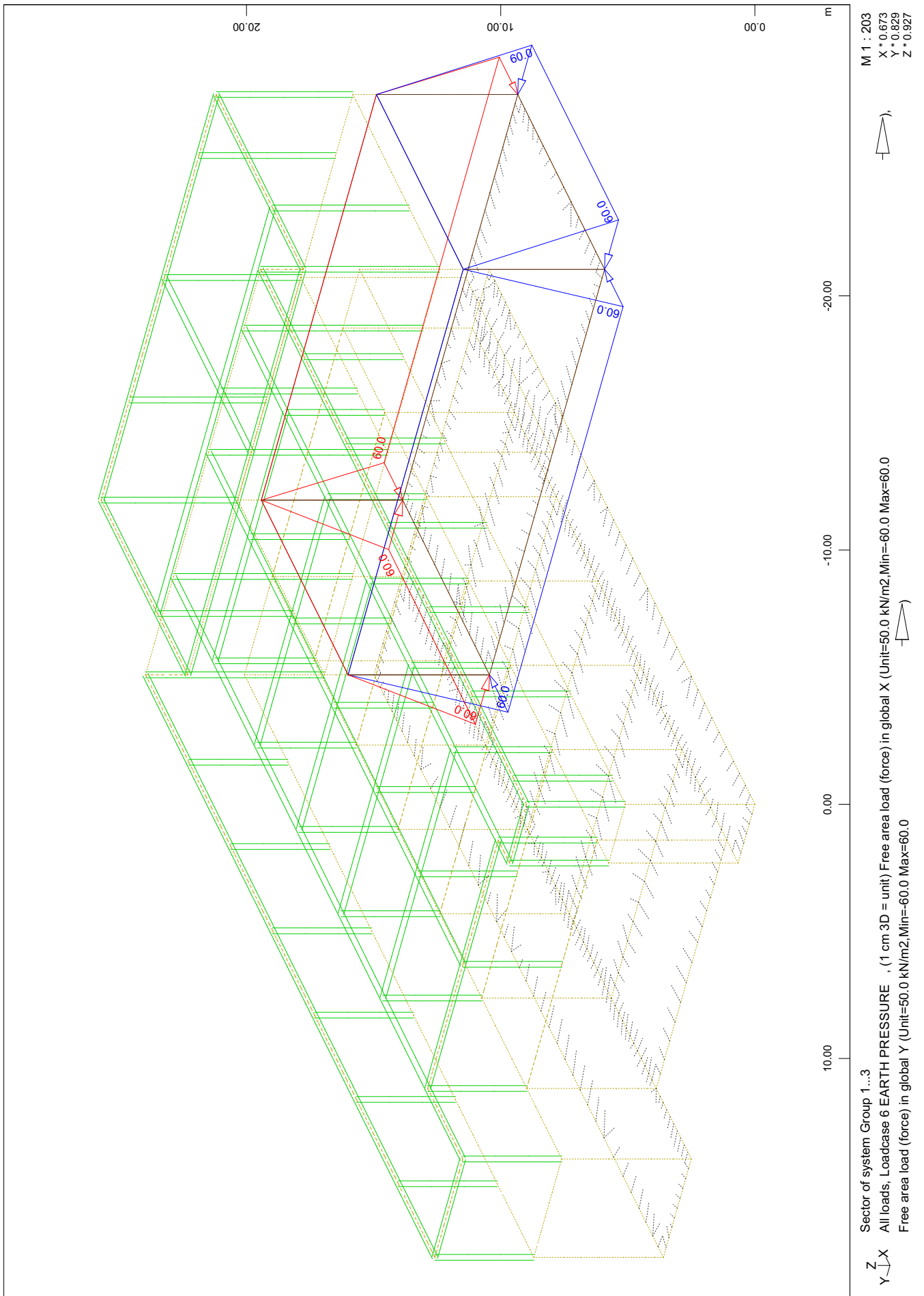


05-ΔΙΥΛΙΣΗ
ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS

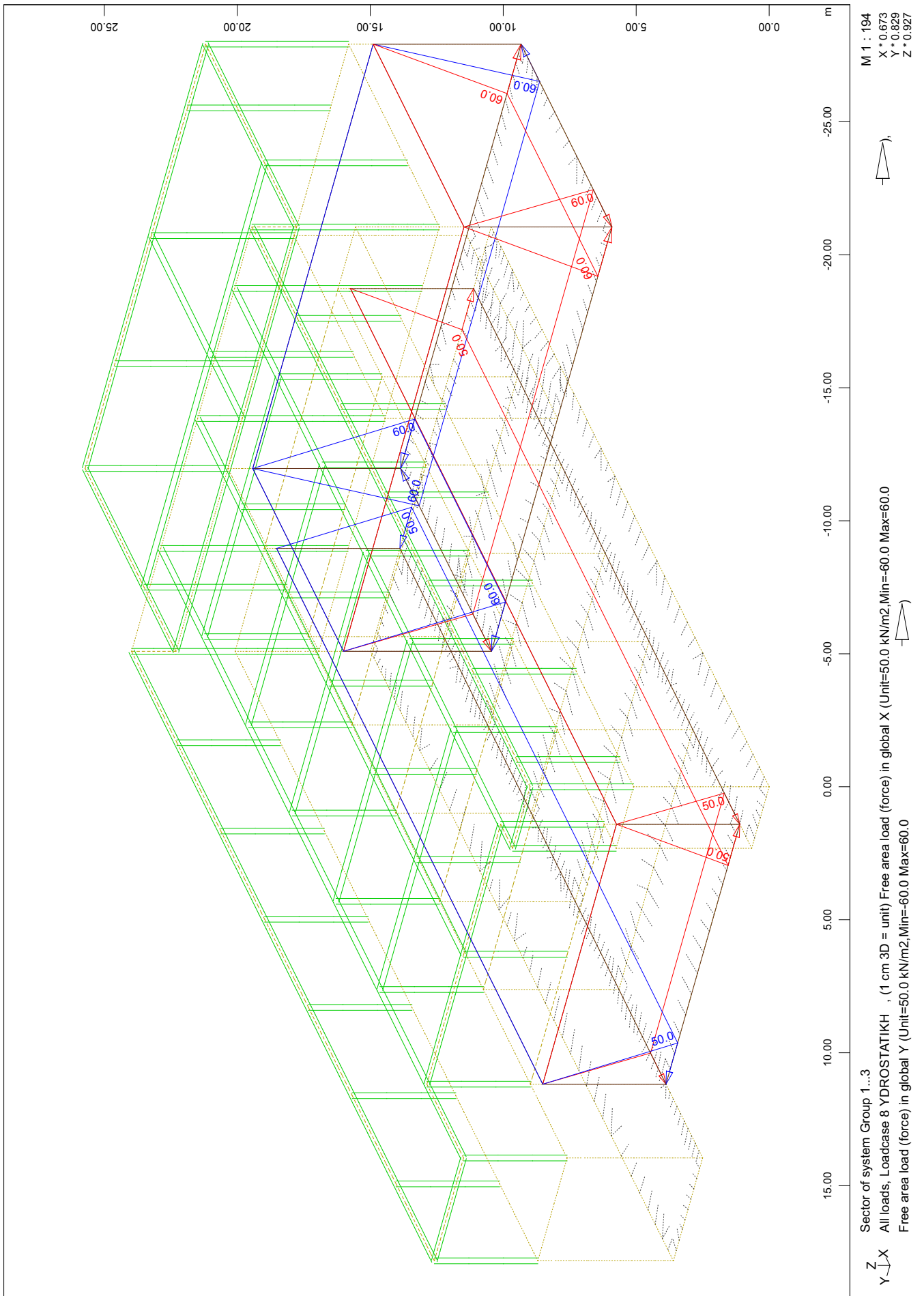
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05-ΔΙΥΛΙΣΗ
ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS



05-ΔΙΥΛΙΣΗ
 ΦΟΡΤΙΑ ΥΠΟΛΟΓΙΣΜΟΥ / LOADS



05-ΔΙΥΛΙΣΗ

design parameter list

Reinforcementparameter two layer reinforcement

Selection Grp elem no. no.	distance		bar-diameter		crackwidth		steelstress		min.reinf.	
	d1-u [mm]	2.lay [mm]	ds-u [mm]	2.lay [mm]	wk-u [mm]	2.lay [mm]	sigsu [MPa]	2.lay [MPa]	asu [cm2/m]	2.lay [cm2/m]
default	30.0	42.0	10	10	0.30	0.30	-	-	-	-
0	30.0	42.0	12	10	0.30	0.30	-	-	-	-
1	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
2	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-

distance upper / lower distance center of bar to surface
 bar-diameter upper / lower bar diameter
 crackwidth upper / lower required crack width
 steelstress upper / lower maximum steel stress in SLS check
 min.reinf. upper / lower minimum reinforcement

The reinforcement directions relate to the local coordinate system of the elements and have to be plotted graphically.

With the input of a steel stress sigsu... the 'crack design according tables' uses this given stress sigsu for the corresponding layer. With this input, the check can be done for bar distances instead of bar diameters.

05-ΔΙΥΛΙΣΗ
 ULS design

Design according to EN 1992-1-1:2004
 Loadcases have been calculated in the Ultimate Limit State
 In BEMESS no additional load safety factor is applied.

Load Cases for the Design

Loadcase	factor	Title
101	1.000	DLZ= -1.35 sum_PZ=-137.4 + Bedding stresses for punching design
102	1.000	DLZ= -1.35 sum_PZ=-137.4 + Bedding stresses for punching design
103	1.000	DLZ= -1.35 sum_PZ=-137.4 + Bedding stresses for punching design
104	1.000	DLZ= -1.35 sum_PZ=-134.2 + Bedding stresses for punching design

Material (EN 1992-1-1:2004)

MAT	fck [N/mm2]	fc [N/mm2]	fctm [N/mm2]	fy [N/mm2]	ft [N/mm2]	N	minT	Type
1	25.0	21.2	2.6			12.9	0.20	
2				500.0	567.5			
3	20.0	20.0	2.2			6.7	0.20	
4	30.0	30.0	2.9			12.5	0.20	
5	25.0	21.2	2.6			6.6	0.20	

MAT material number
 fck nominal strength of the concrete
 fc strength of the concrete
 fctm tensile strength of the concrete
 fy yield stress reinforcing steel
 ft tensile stress reinforcing steel
 N ratio Young's modules steel/concrete
 minT minimum transverse reinforcement
 Type character of the loading

Minimum reinforcement: 0.00 % of statically required section
 Reduction of FC in case of transvers tension = 25.0 [o/o]

Material-safety-factors:

MAT	concr SC1	SC2	steel SS1	SS2
1	1.50	1.50		
2			1.15	1.15
3	1.50	1.50		
4	1.50	1.50		
5	1.50	1.50		

MAT material number
 concr material safety SC1/SC2 = bending/compression
 steel material safety steel bending/compression

At direct supports from the face of the support up to 1.0*d the shear force is reduced.
 The maximum shear capacity is checked at the face of the support without reduction.
 For punching design, the longitudinal reinforcement will be increased up to 1.50% to avoid shear reinforcement [input PUNC...RO_V].
 Outside the punching area, the normal slab shear design may increase the, longitudinal reinforcement up to 0.20% [input CTRL...RO_V].

Reinforcementparameter two layer reinforcement

Selection	distance		bar-diameter		crackwidth		steelstress		min.reinf.	
Grp elem	d1-u	2.lay	ds-u	2.lay	wk-u	2.lay	sigsu	2.lay	asu	2.lay
no. no.	d1-l	2.lay	ds-l	2.lay	wk-l	2.lay	sigsl	2.lay	asl	2.lay
	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[MPa]	[MPa]	[cm2/m]	[cm2/m]
default	30.0	42.0	10	10	0.30	0.30	-	-	-	-
	30.0	42.0	12	10	0.30	0.30	-	-	-	-
0	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
1	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
2	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-

distance upper / lower distance center of bar to surface
 bar-diameter upper / lower bar diameter
 crackwidth upper / lower required crack width
 steelstress upper / lower maximum steel stress in SLS check
 min.reinf. upper / lower minimum reinforcement

The reinforcement directions relate to the local coordinate system of the elements and have to be plotted graphically.
 With the input of a steel stress sigsu... the 'crack design according tables' uses this given stress sigsu for the corresponding layer. With this input, the check can be done for bar distances instead of bar diameters.
 The reinforcement is saved in the data base as design case 1

At punching-nodes the bending moments have been reduced (rounded)
 At column-nodes the slab-thickness for bending-design has been increased with 1:3 starting at the column-edge (not at wall punching nodes)

05-ΔΙΥΛΙΣΗ
 ULS design

Design according to EN 1992-1-1:2004
 Loadcases have been calculated in the Ultimate Limit State
 In BEMESS no additional load safety factor is applied.

Load Cases for the Design

Loadcase	factor	Title
201	1.000	EQ_Y-Y q=3.00 + Bedding stresses for punching design
202	1.000	EQ_X-X q=3.00 + Bedding stresses for punching design

Material (EN 1992-1-1:2004)

MAT	fck [N/mm2]	fc [N/mm2]	fctm [N/mm2]	fy [N/mm2]	ft [N/mm2]	N	minT	Type
1	25.0	21.2	2.6			12.9	0.20	
2				500.0	567.5			
3	20.0	20.0	2.2			6.7	0.20	
4	30.0	30.0	2.9			12.5	0.20	
5	25.0	21.2	2.6			6.6	0.20	

MAT material number
 fck nominal strength of the concrete
 fc strength of the concrete
 fctm tensile strength of the concrete
 fy yield stress reinforcing steel
 ft tensile stress reinforcing steel
 N ratio Young's modules steel/concrete
 minT minimum transverse reinforcement
 Type character of the loading

Minimum reinforcement: 0.00 % of statically required section
 Reduction of FC in case of transvers tension = 25.0 [o/o]

Material-safety-factors:

MAT	concr	SC1	SC2	steel	SS1	SS2
1		1.50	1.50			
2				1.15	1.15	
3		1.50	1.50			
4		1.50	1.50			
5		1.50	1.50			

MAT material number
 concr material safety SC1/SC2 = bending/compression
 steel material safety steel bending/compression

At direct supports from the face of the support up to 1.0*d the shear force is reduced.

The maximum shear capacity is checked at the face of the support without reduction.
 For punching design, the longitudinal reinforcement will be increased up to 1.50% to avoid shear reinforcement [input PUNC...RO_V].

Outside the punching area, the normal slab shear design may increase the, longitudinal reinforcement up to 0.20% [input CTRL...RO_V].

Reinforcementparameter two layer reinforcement

Selection Grp elem no. no.	distance		bar-diameter		crackwidth		steelstress		min.reinf.	
	d1-u	2.lay	ds-u	2.lay	wk-u	2.lay	sigsu	2.lay	asu	2.lay
	d1-l	2.lay	ds-l	2.lay	wk-l	2.lay	sigsl	2.lay	asl	2.lay
	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[MPa]	[MPa]	[cm2/m]	[cm2/m]
default	30.0	42.0	10	10	0.30	0.30	-	-	-	-
	30.0	42.0	12	10	0.30	0.30	-	-	-	-
0	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
1	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
2	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-

distance upper / lower distance center of bar to surface
 bar-diameter upper / lower bar diameter
 crackwidth upper / lower required crack width
 steelstress upper / lower maximum steel stress in SLS check
 min.reinf. upper / lower minimum reinforcement

The reinforcement directions relate to the local coordinate system of the elements and have to be plotted graphically.

With the input of a steel stress sigsu... the 'crack design according tables' uses this given stress sigsu for the corresponding layer. With this input, the check can be done for bar distances instead of bar diameters.

The reinforcement is saved in the data base as design case 2

At punching-nodes the bending moments have been reduced (rounded)

At column-nodes the slab-thickness for bending-design has been increased with 1:3 starting at the column-edge (not at wall punching nodes)

05-ΔΙΥΛΙΣΗ
 SLS design

Maximum of reinforcement-distributions

The reinforcement maximum was build out of the numbers of reinforcement-distributions:

1

and stored as new reinforcement-distribution 3 .

Design according to EN 1992-1-1:2004

Loadcases have been calculated in the Serviceability State

In BEMESS no additional load safety factor is applied.

Load Cases for the Design

Loadcase	factor	Title
301	1.000	DLZ= -1.00 sum_PZ=-101.0 + Bedding stresses for punching design

Load Cases - with factors of dead load in per cent

LcNo per cent LcNo per cent LcNo per cent LcNo per cent LcNo per cent

301 100.0

Material (EN 1992-1-1:2004)

MAT	fck	fc	fctm	fy	ft	N	minT	Type
	[N/mm2]	[N/mm2]	[N/mm2]	[N/mm2]	[N/mm2]			
1	25.0	21.2	2.6			12.9	0.20	
2				500.0	567.5			
3	20.0	20.0	2.2			6.7	0.20	
4	30.0	30.0	2.9			12.5	0.20	
5	25.0	21.2	2.6			6.6	0.20	

MAT material number
 fck nominal strength of the concrete
 fc strength of the concrete
 fctm tensile strength of the concrete
 fy yield stress reinforcing steel
 ft tensile stress reinforcing steel
 N ratio Young's modules steel/concrete
 minT minimum transverse reinforcement
 Type character of the loading

Minimum reinforcement: 0.00 % of statically required section

A robustness minimum reinforcement has not been requested [MREI] and has to be checked separately.

A minimum reinforcement has not been requested [MREI] and has to be checked separately.

SERVICEABILITY LIMIT STATE CONTROL PARAMETERS

No Code dNW [mm] wk [mm]

1 EN-1992 ->para ->para

Calculation of crack-width acc." EN 1992 7.3.4

Reinforcementparameter two layer reinforcement

Selection Grp elem	distance		bar-diameter		crackwidth		steelstress		min.reinf.	
	d1-u	2.lay	ds-u	2.lay	wk-u	2.lay	sigsu	2.lay	asu	2.lay
no. no.	d1-l	2.lay	ds-l	2.lay	wk-l	2.lay	sigsl	2.lay	asl	2.lay
	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[MPa]	[MPa]	[cm2/m]	[cm2/m]
default	30.0	42.0	10	10	0.30	0.30	-	-	-	-
	30.0	42.0	12	10	0.30	0.30	-	-	-	-
0	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
1	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-
2	35.0	45.0	10	10	0.15	0.15	-	-	-	-
	35.0	45.0	10	10	0.15	0.15	-	-	-	-

distance upper / lower distance center of bar to surface
 bar-diameter upper / lower bar diameter
 crackwidth upper / lower required crack width
 steelstress upper / lower maximum steel stress in SLS check
 min.reinf. upper / lower minimum reinforcement

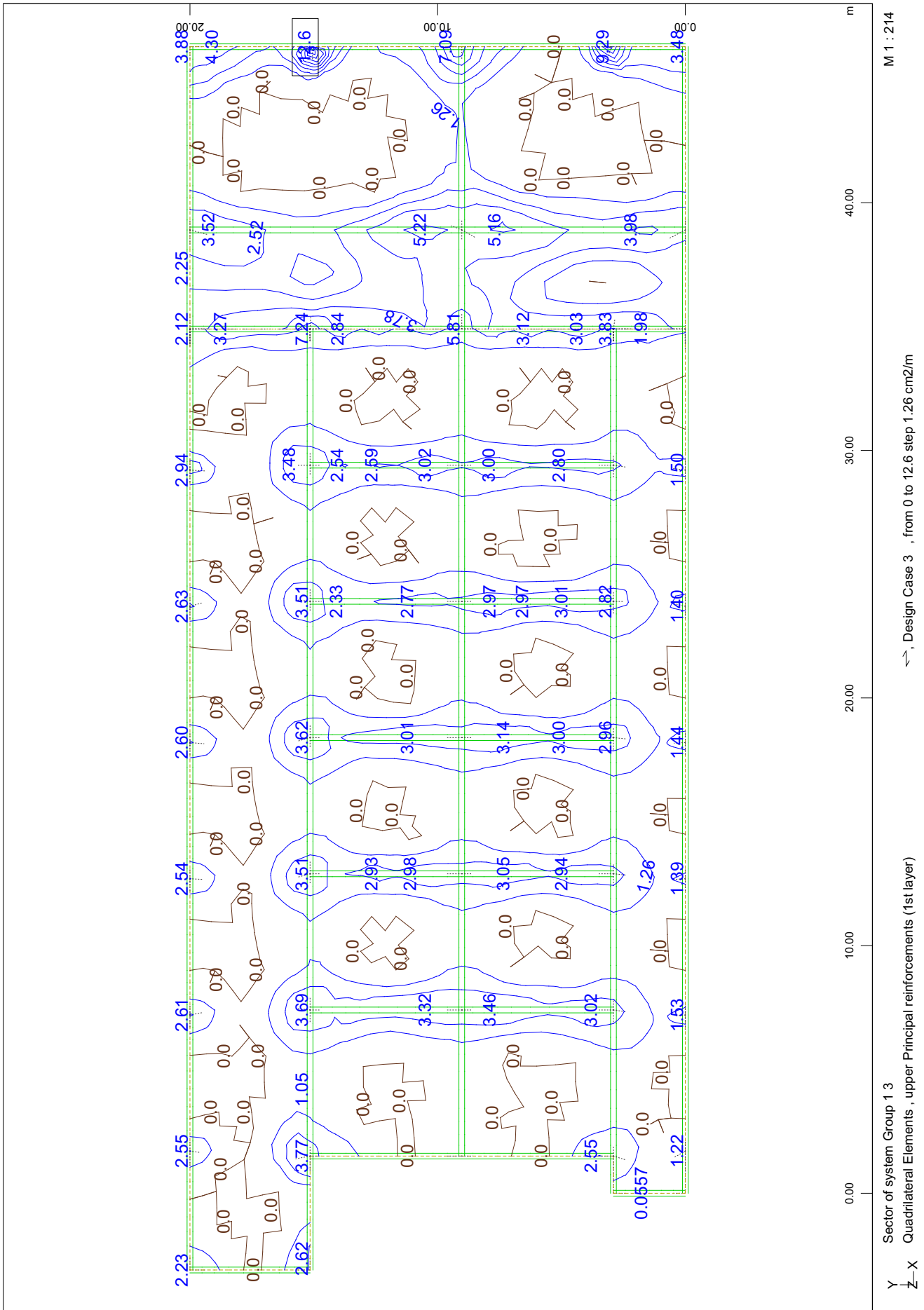
The reinforcement directions relate to the local coordinate system of the elements and have to be plotted graphically.

With the input of a steel stress sigsu... the 'crack design according tables' uses this given stress sigsu for the corresponding layer. With this input, the check can be done for bar distances instead of bar diameters.

The reinforcement is saved in the data base as design case 3

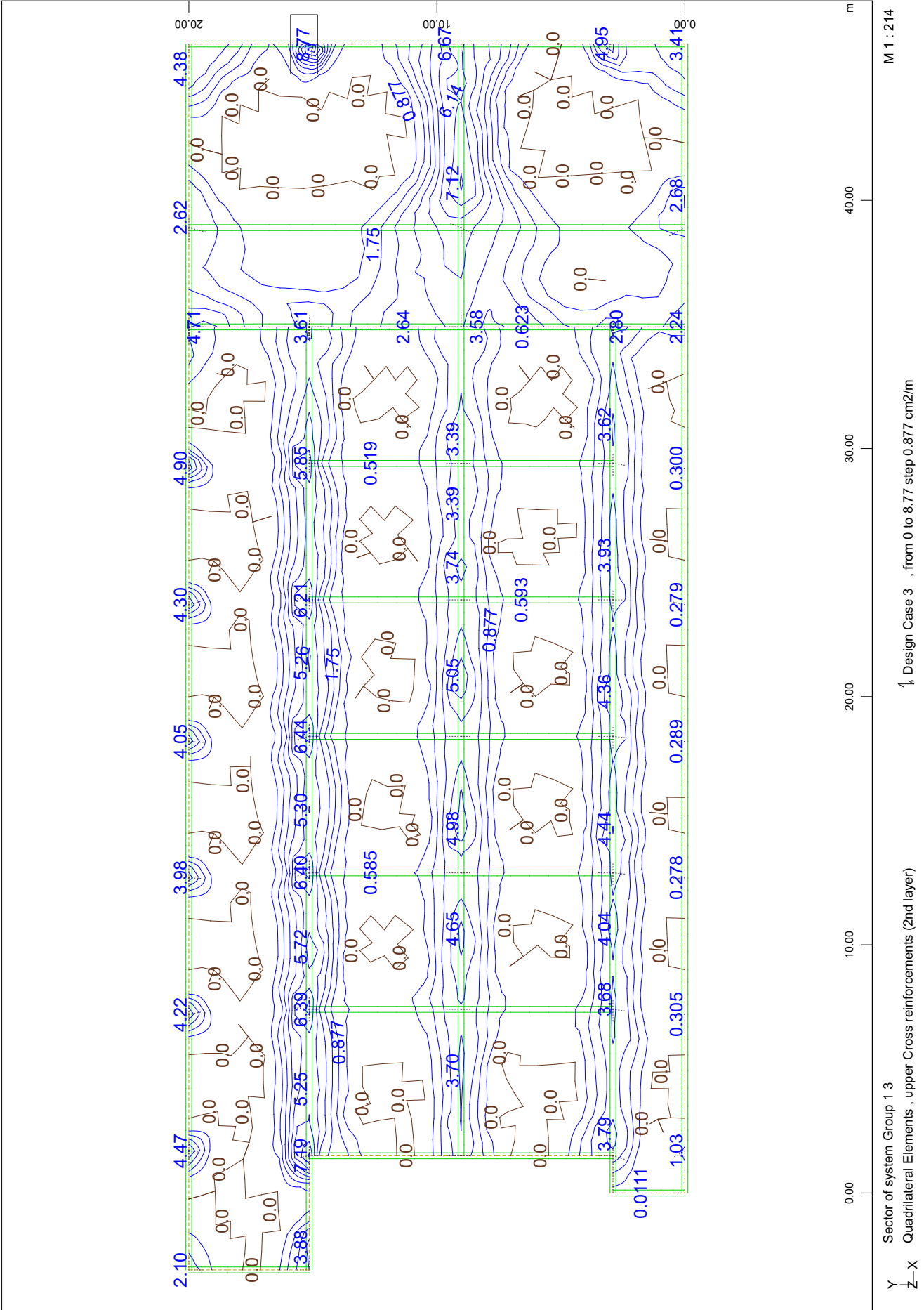
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΟΡΟΦΗΣ/ROOF SLABS REINFORCEMENTS
 ΟΚΛ/SL5 : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)

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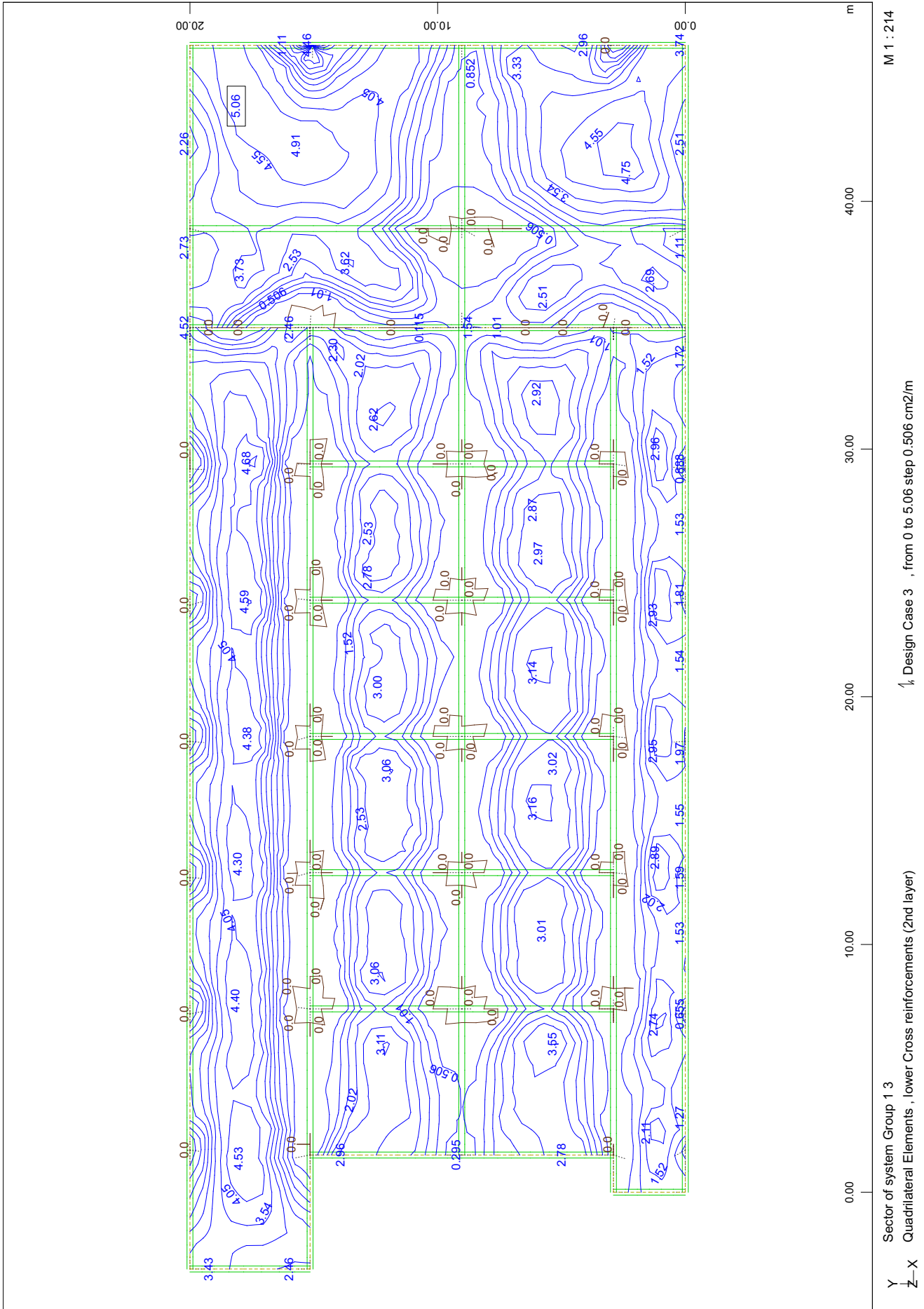


↔, Design Case 3 , from 0 to 12.6 step 1.26 cm2/m

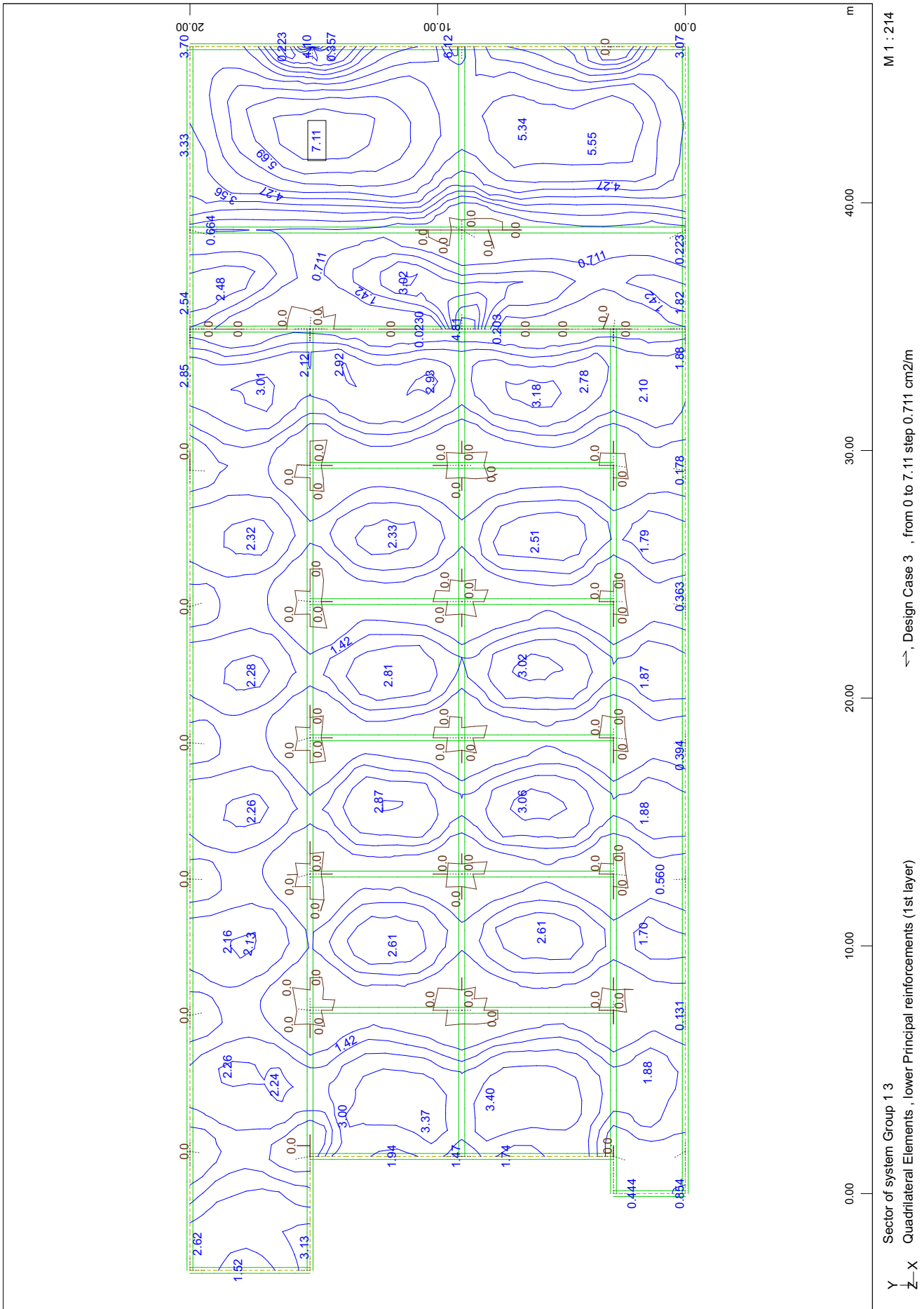
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΟΡΟΦΗΣ/ROOF SLABS REINFORCEMENTS
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



05-ΔΙΥΛΙΣΗ
ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΟΡΟΦΗΣ/ROOF SLABS REINFORCEMENTS
ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)

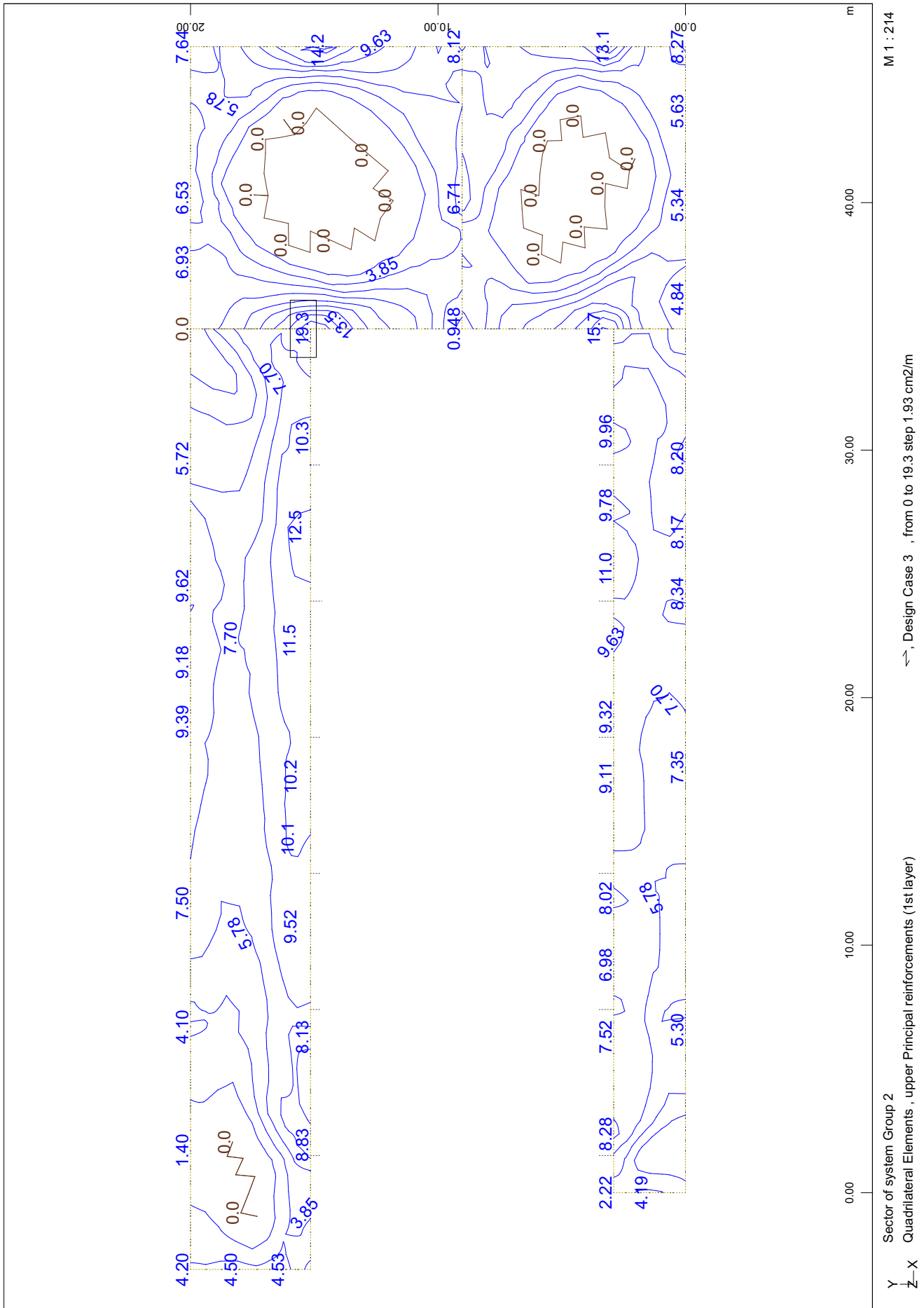


05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΟΡΟΦΗΣ/ROOF SLABS REINFORCEMENTS
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)

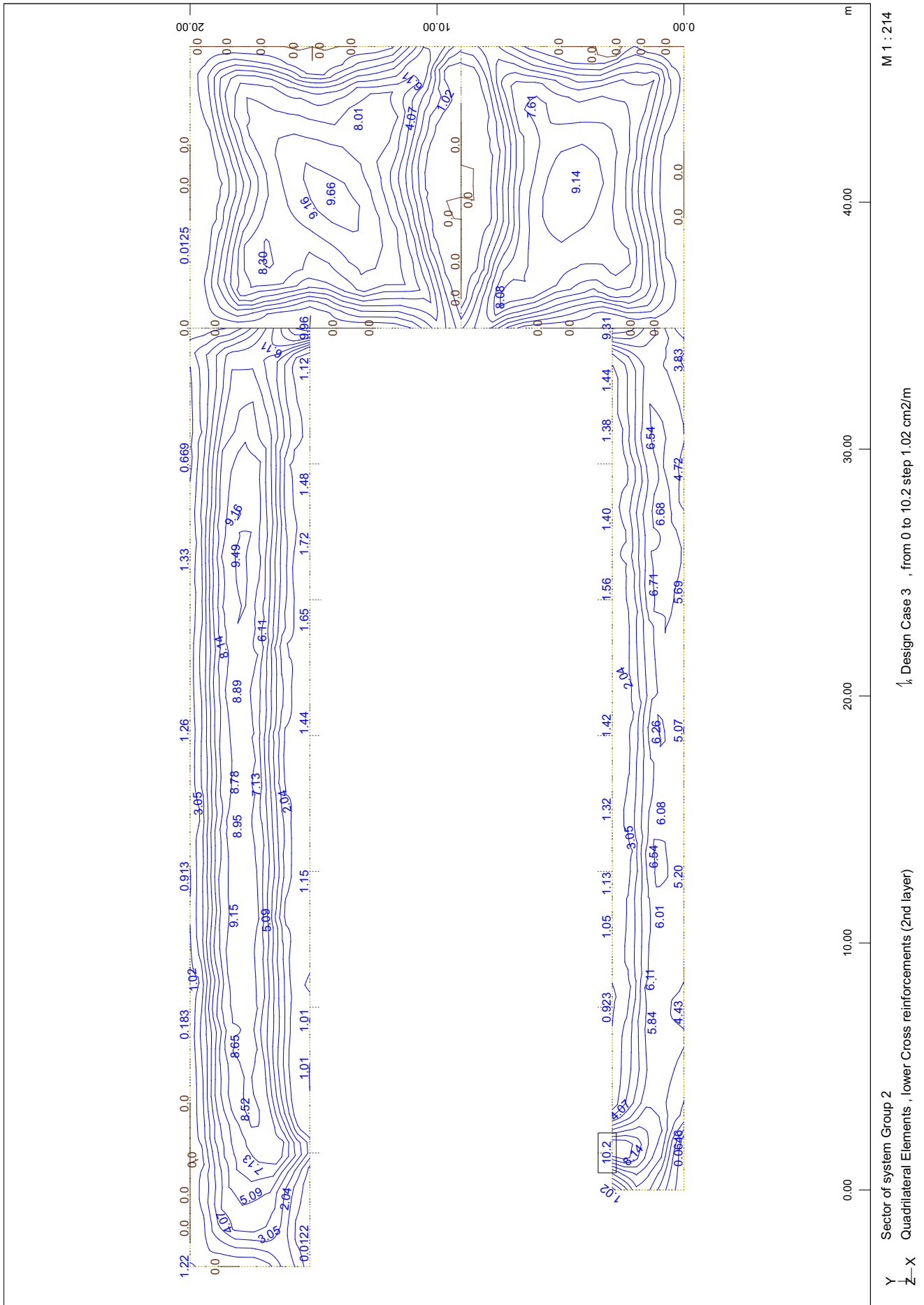
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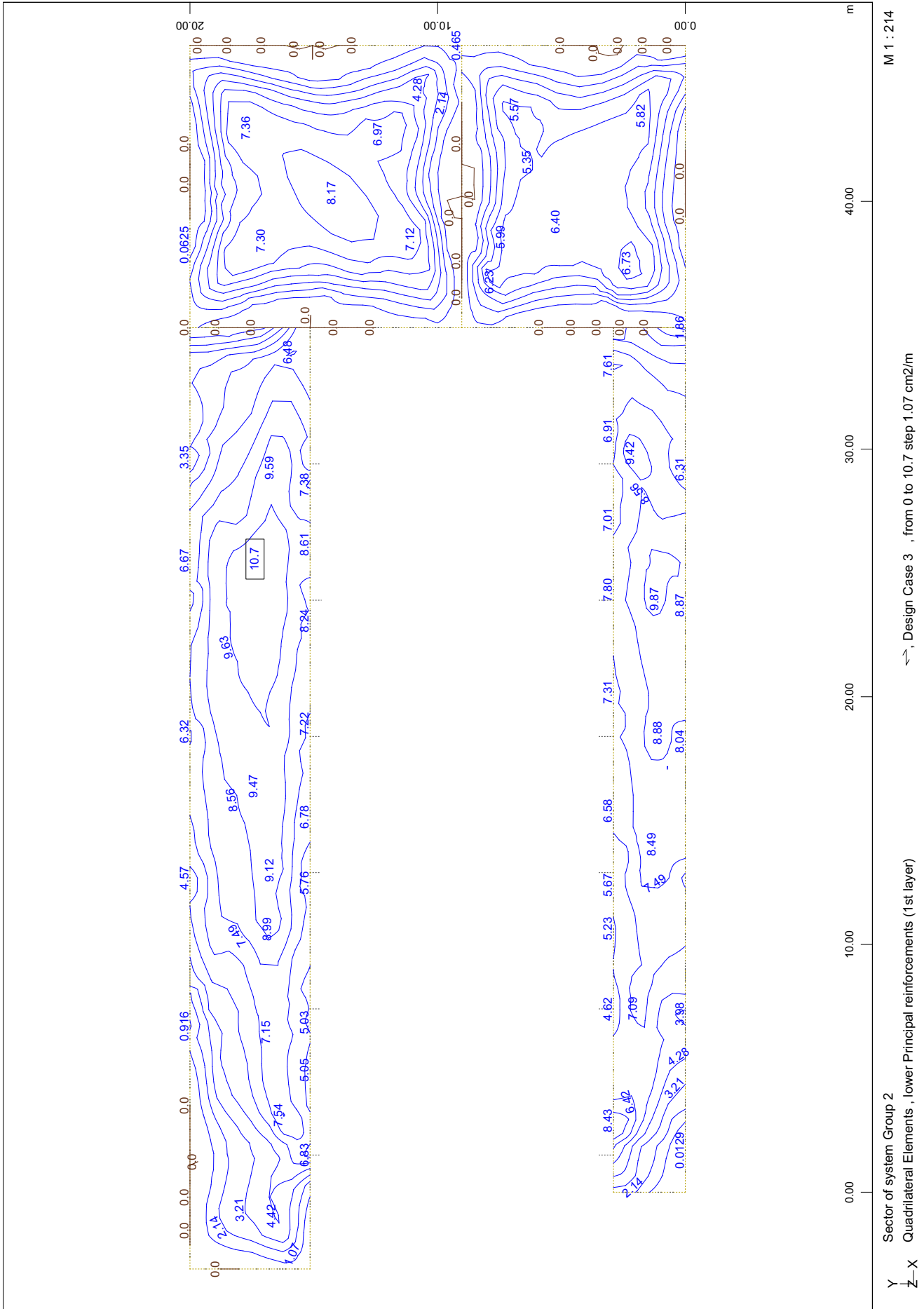
05-ΔΙΥΛΙΣΗ

ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC

ΟΚΛ/ΣΛΣ : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)

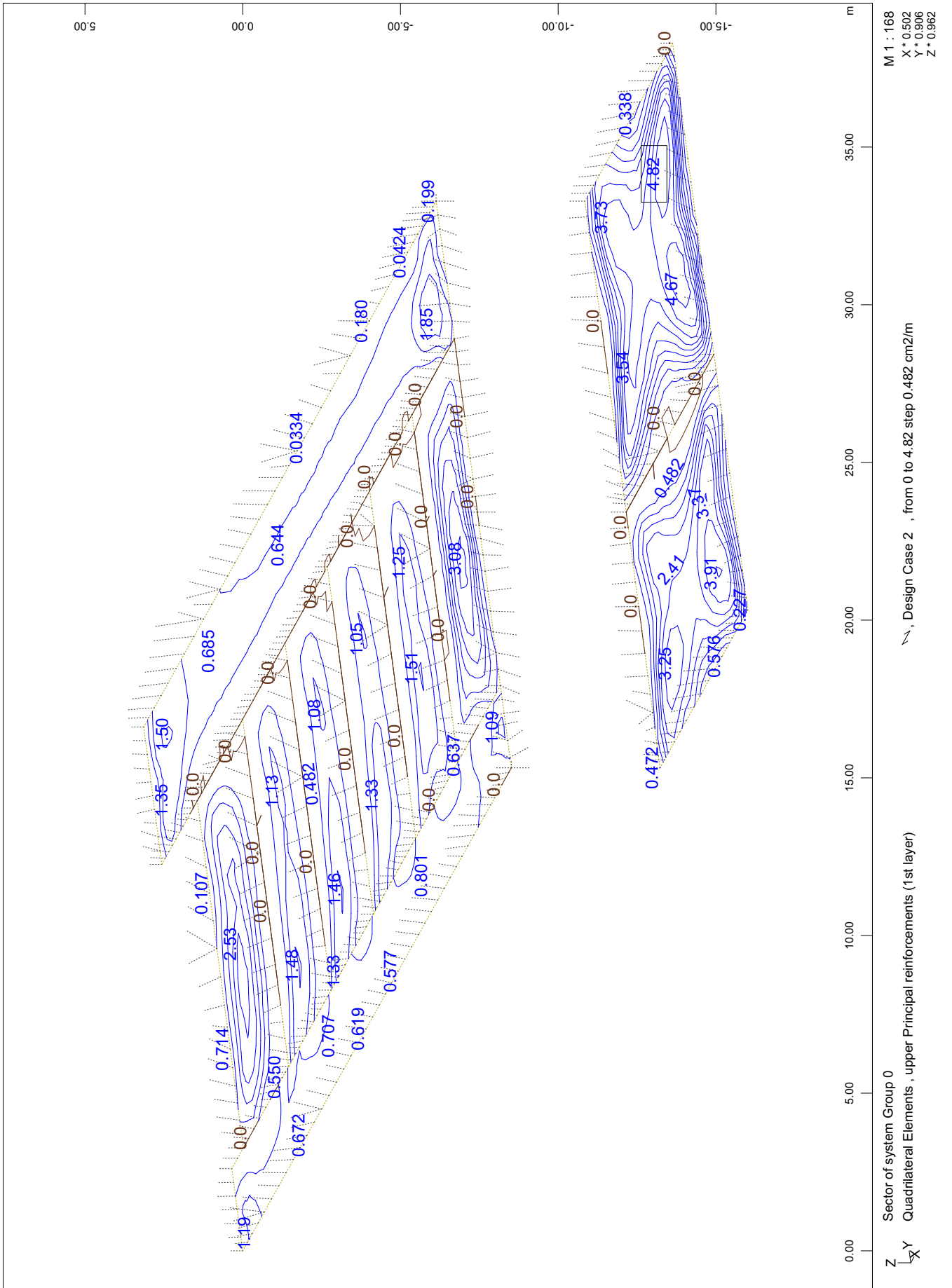


05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΠΛΑΚΩΝ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΛ/ΣΛΣ : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



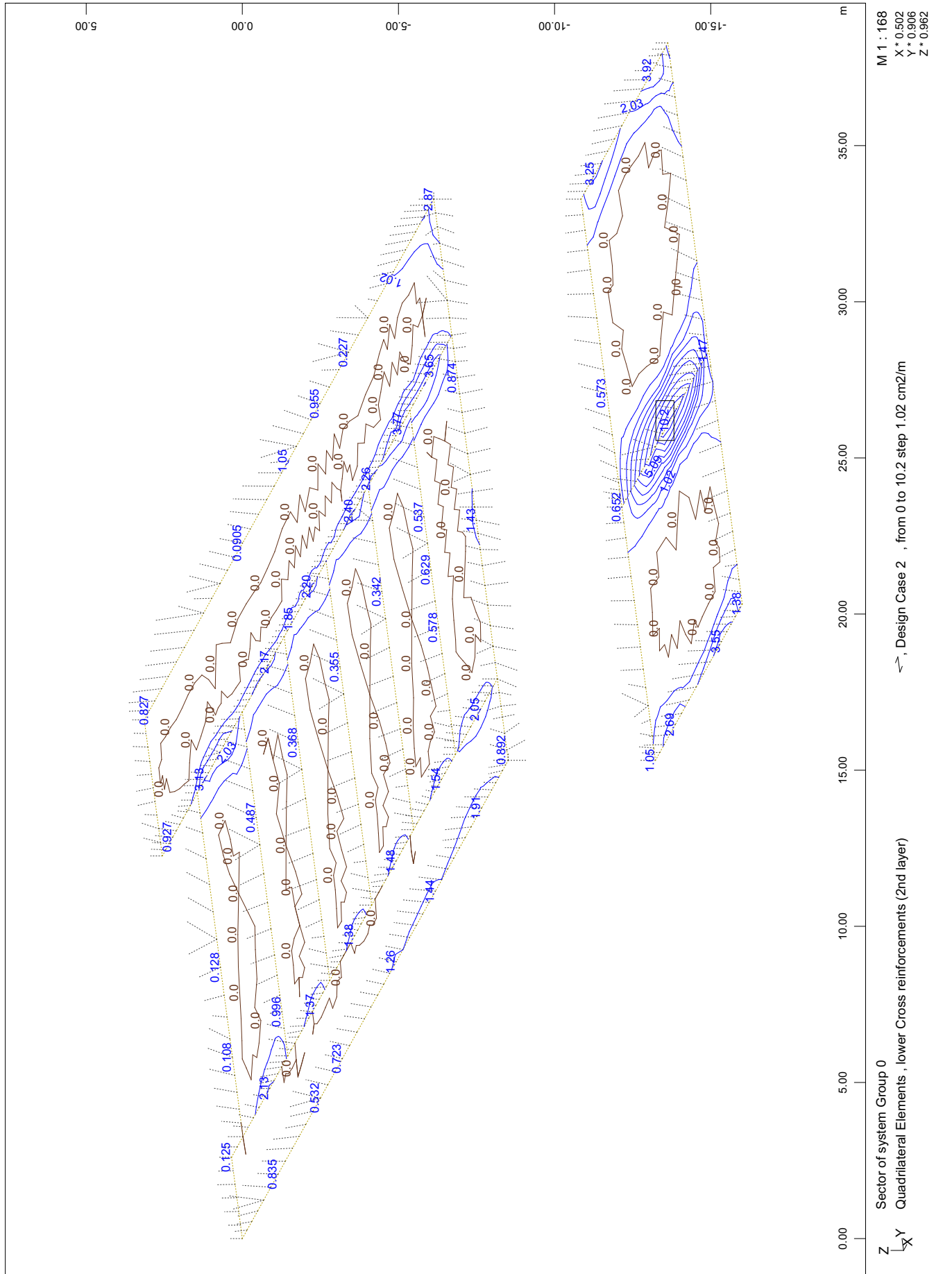
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 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/ΕQ) : LCR 2

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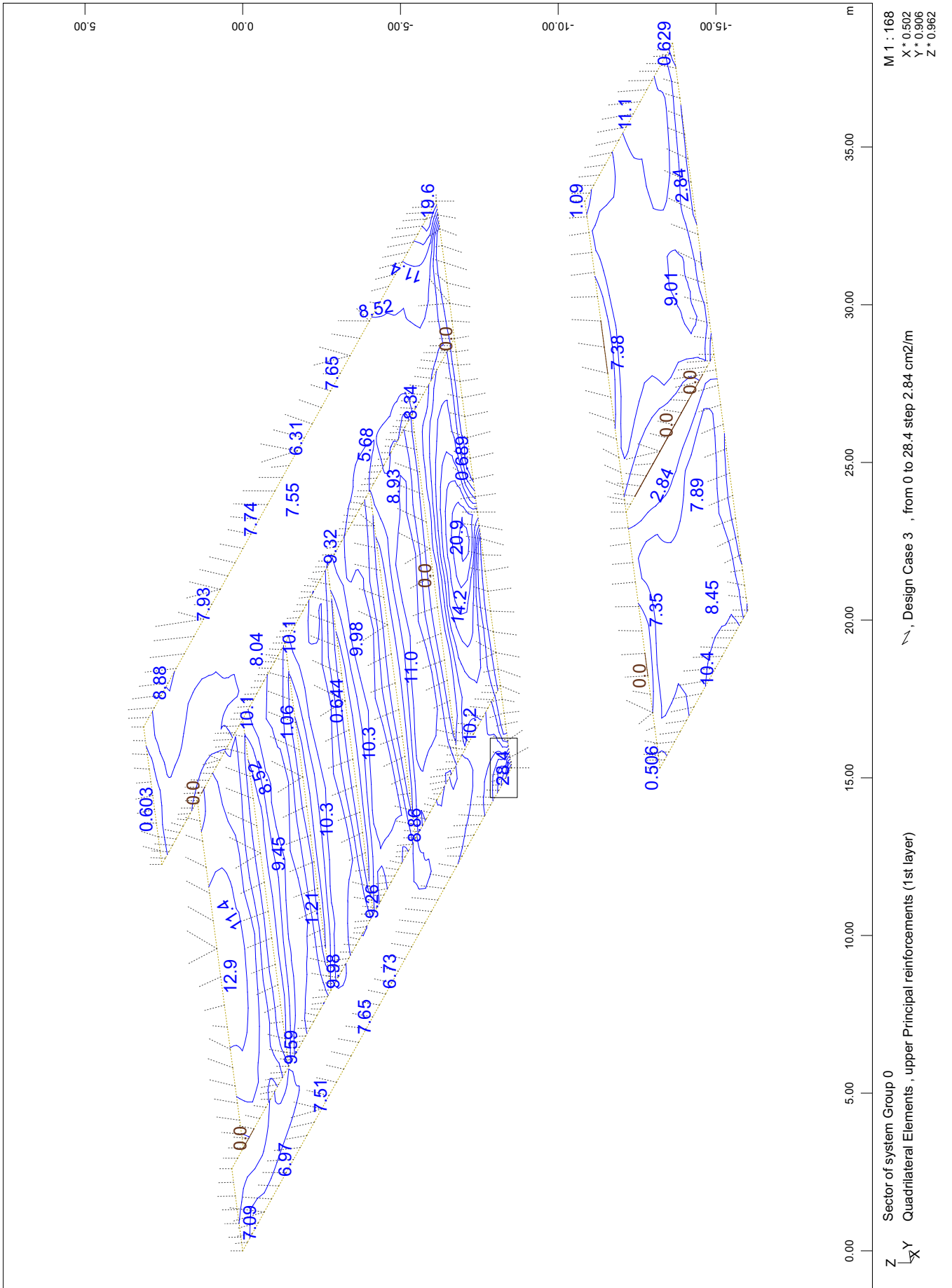
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΑ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/ΕQ) : LCR 2

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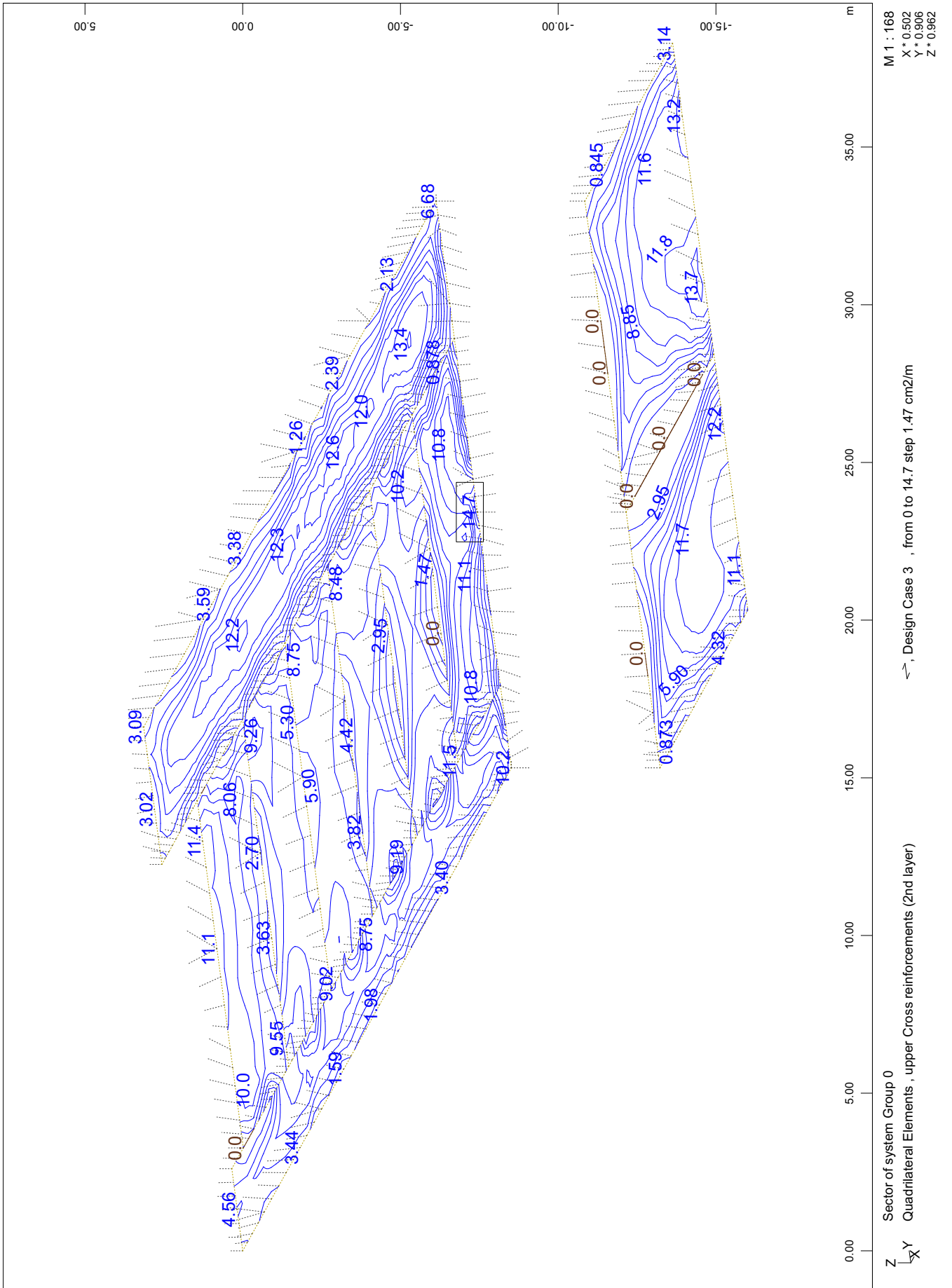
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/ΕQ) : LCR 2

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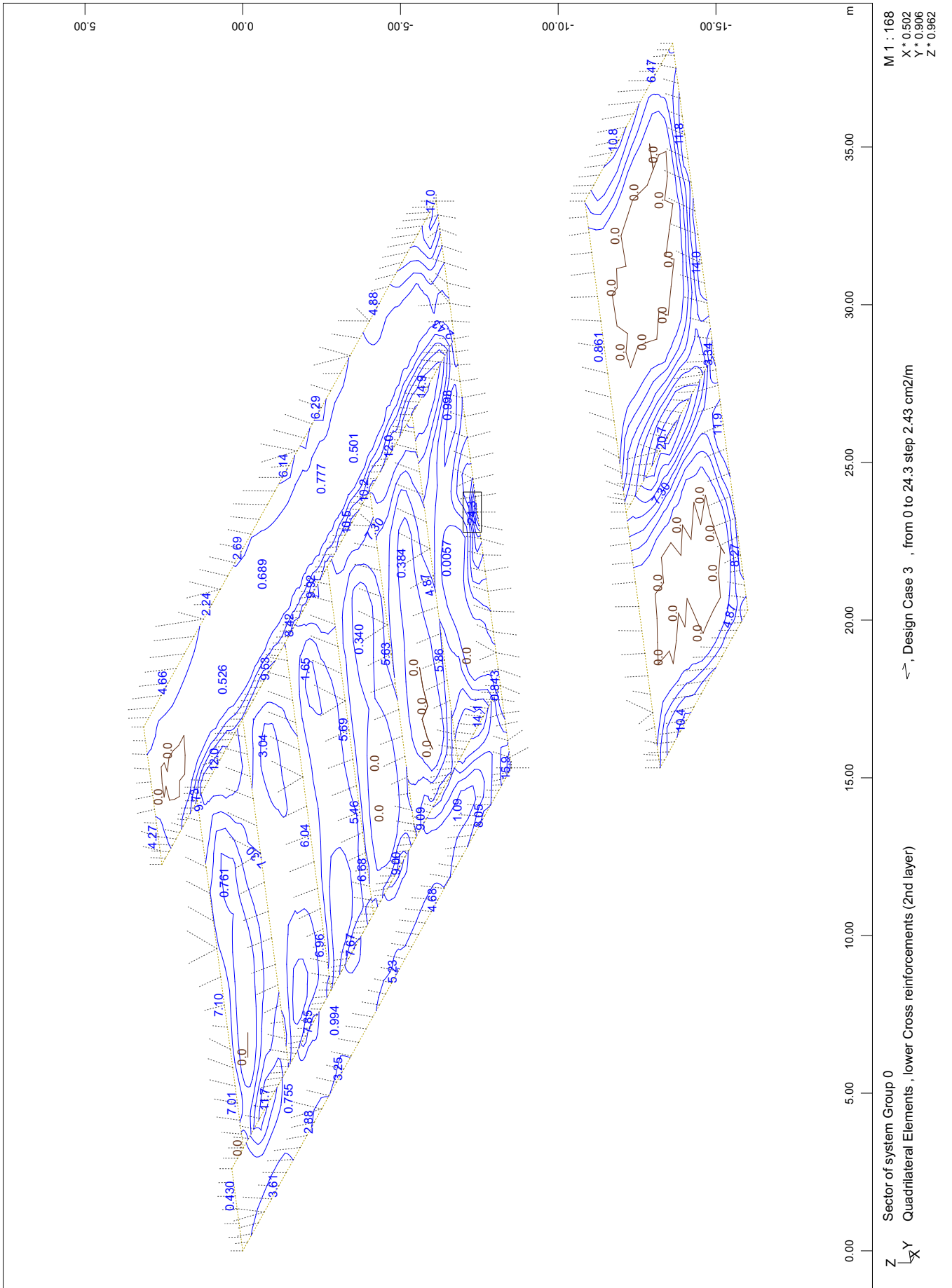
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 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΑ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/EQ) : LCR 2

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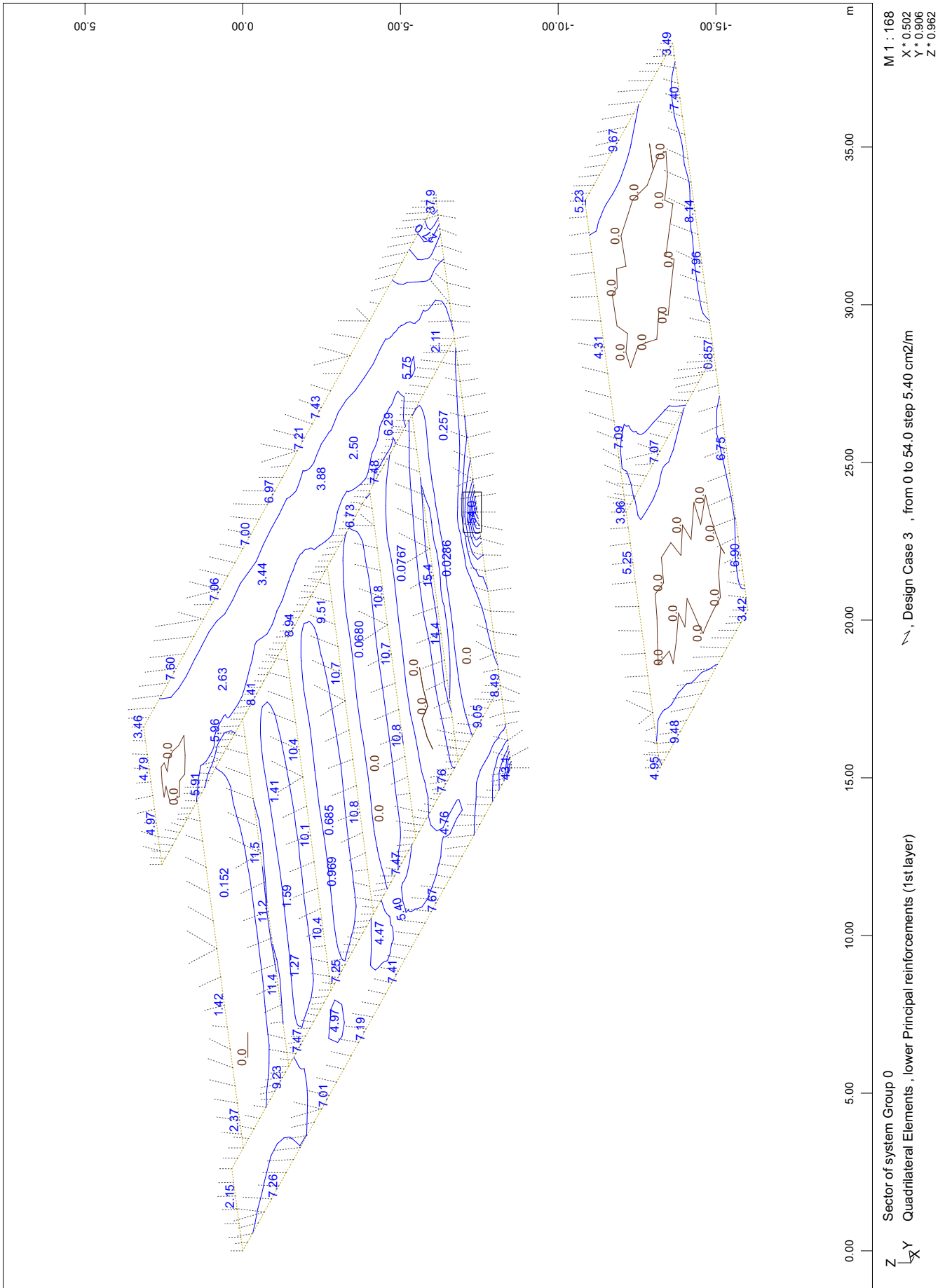
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΑ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/ΕQ) : LCR 2

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05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΘΕΜΕΛΙΩΣΗΣ ΥΠΟΓΕΙΟΥ / BASEMENT SLABS REINFORC
 ΟΚΛ/SLS : LCR 3 (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)
 ΟΚΑ/ULS (ΣΕΙΣΜΟΣ/ΕQ) : LCR 2

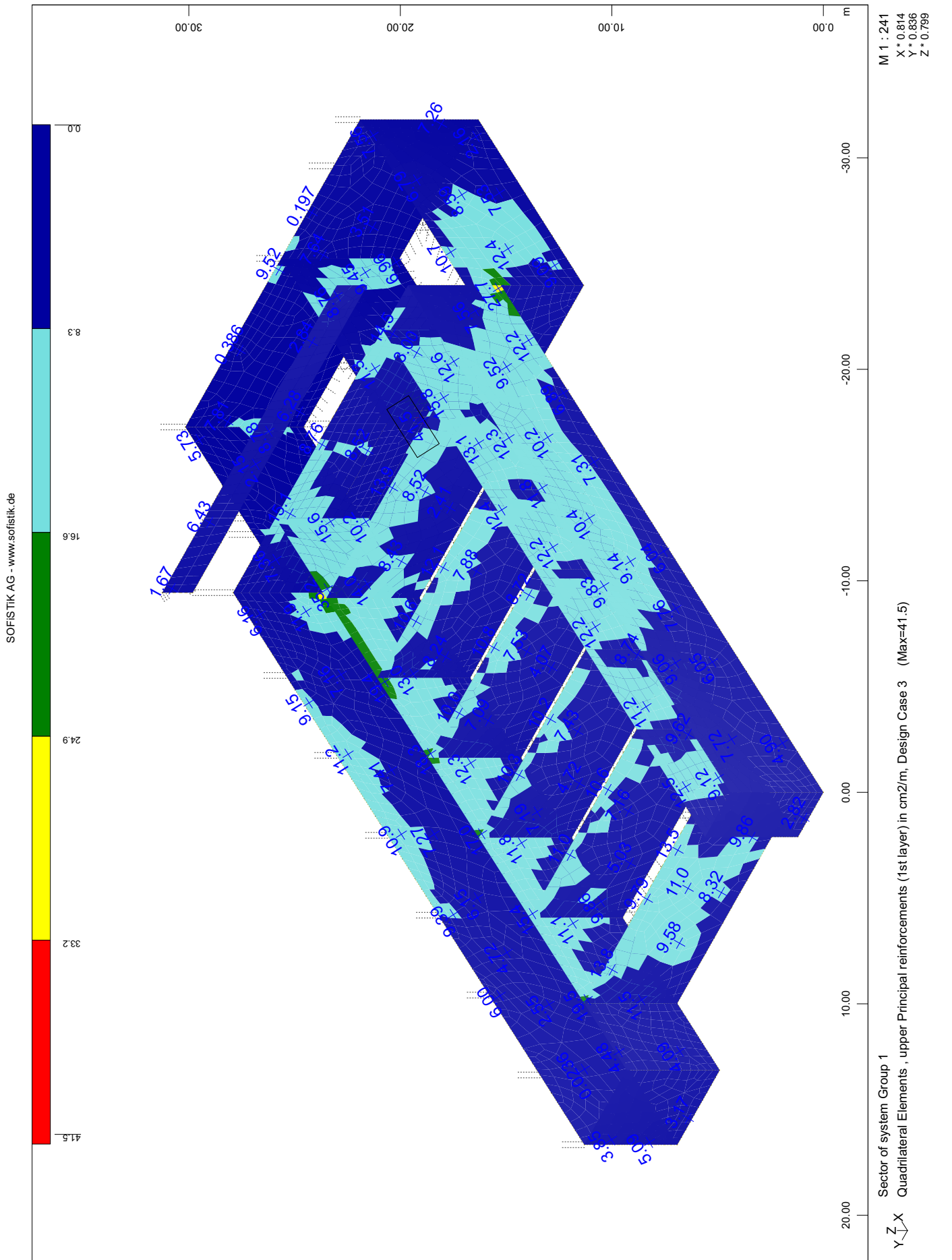
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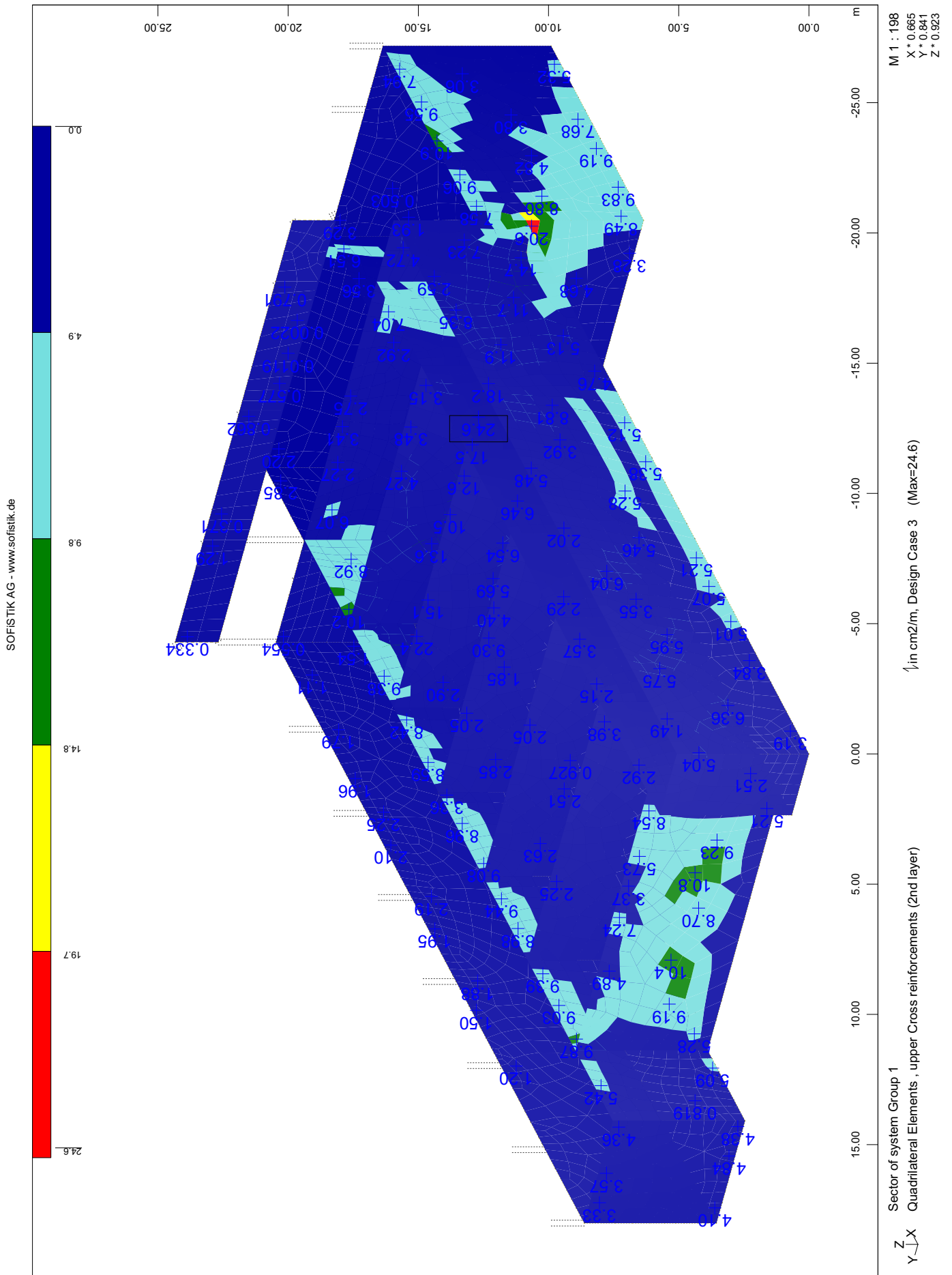
05-ΔΙΥΛΙΣΗ

ΟΠΛΙΣΜΟΙ ΤΟΙΧΩΜΑΤΩΝ ΔΕΞΑΜΕΝΩΝ/TANK WALLS REINFORCEMENTS

ΟΚΛ/SLS : LCR 3 (wk<0.20mm) (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



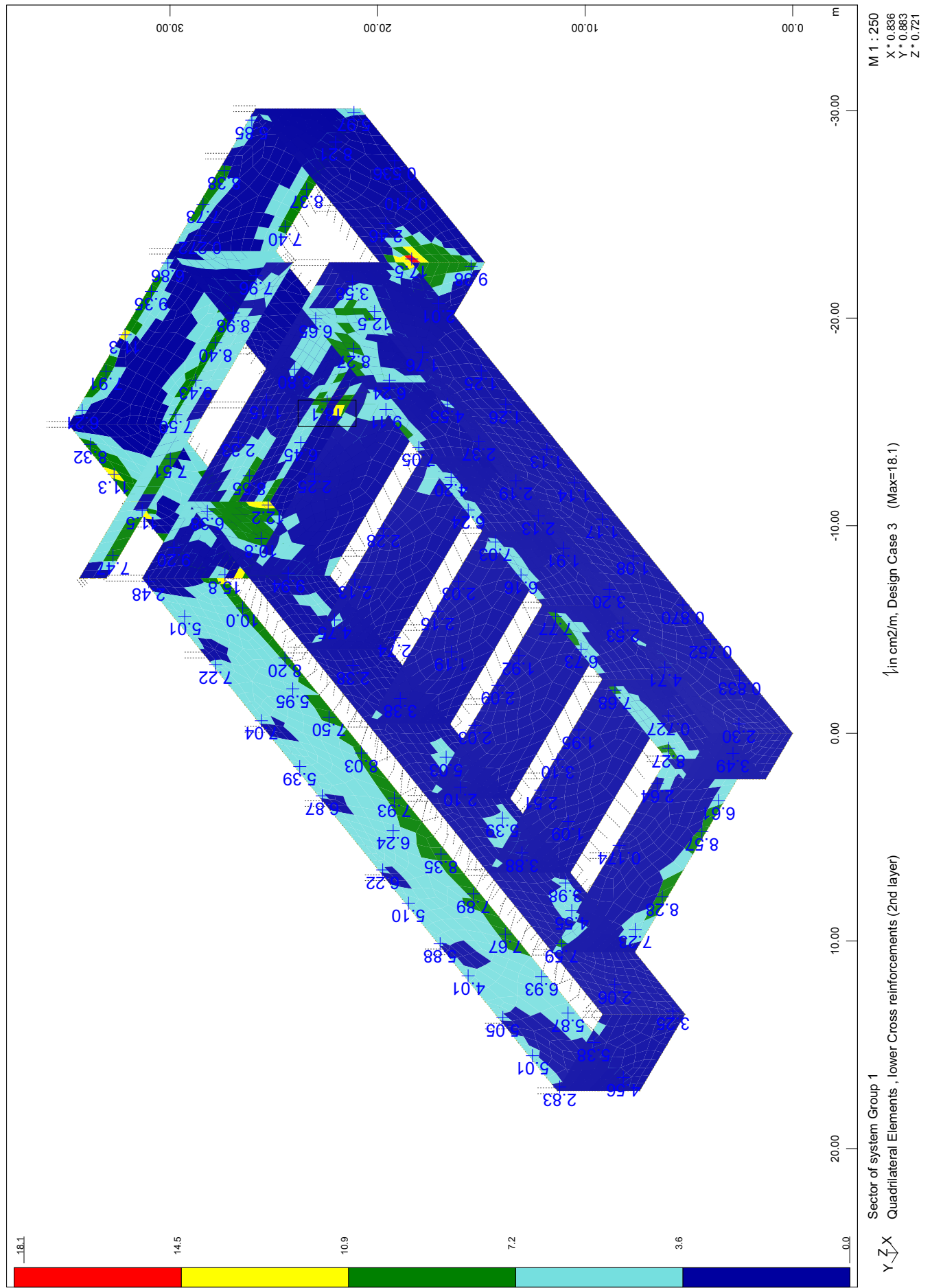
05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΤΟΙΧΩΜΑΤΩΝ ΔΕΞΑΜΕΝΩΝ/TANK WALLS REINFORCEMENTS
 ΟΚΛ/SLS : LCR 3 (Wk<0.20mm) (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



05-ΔΙΥΛΙΣΗ

ΟΠΛΙΣΜΟΙ ΤΟΙΧΩΜΑΤΩΝ ΔΕΞΑΜΕΝΩΝ/TANK WALLS REINFORCEMENTS

ΟΚΛ/SLS : LCR 3 (wk<0.20mm) (ΟΚΑ LCR 1 ΠΕΡΙΛΑΜΒΑΝΕΤΑΙ/ULS INCLUDED)



05-ΔΙΥΛΙΣΗ
 ULS design beams

Selected Beam Elements

FROM	TO	INC	X-VALUE	NC	MEMBER	CS0	CS1	CS2	CS3	CS4	CS5
all elements											

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992) DUMMY

All moments will be smoothed out between face and support
 Reinforcement will be accounted for sectional values as defined in AQUA
 Reinforcements saved as design case LCR 10

Considered Load Cases

101	102	103	104
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Ultimate Load Design

Design for ultimate loads EuroNorm EN 1992 (2004) Concrete Structures
 Biaxial bending

Safety factors	SC-1	SC-2	SC-S	SS-1	SS-2	SS-S	PIIa
	1.50	1.50	1.50	1.15	1.15	1.00	7
Strain limits	C1	C2	S1	S2	Z1	Z2	
max	-3.50	-2.00	δ= 1.00	45.00	-3.50	20.00	

parameters for reinforcements

Minimum reinforcements	compression	min. reinforcem.	maximum-
Bending. Compress.	e/d	N/Npl	requ. section
0.13 [o/o]	0.20 [o/o]	3.50	0.0010
		0.00	0.10
			8.00

Tensile forces in the longitudinal reinforcements due to shear are NOT accounted for.

Material of sections uses Ultimate Limit strain-stress law with individual safety factors
 Material of reinforcements uses Ultimate Limit strain-stress law with individual safety factors

MNo.	temp lev.	Material-safety [-]	max.compr stress [MPa]	at strain [o/oo]	max.tens stress [MPa]	at strain [o/oo]	tension-stiffening [MPa]
1	0	1.500	-14.17	-2.00	0.00	0.00	
2	0	1.150	-500.00	-75.00	500.00	75.00	
3	0	1.500	-13.33	-2.00	0.00	0.00	
4	0	1.500	-20.00	-2.00	0.00	0.00	
5	0	1.500	-14.17	-2.00	0.00	0.00	

Shear Design

Design for shear Eurocode EN 1992 (2004)
 Minimum shear factor or tan of inclination of compressive struts 0.40 / 1.00

MNo	f-cd [MPa]	tau-rd [MPa]	sigIIQ [MPa]	sigIIIT [MPa]	sigIIQ+T [MPa]	fyd [MPa]
1	14.17	0.12	7.65	7.65	7.65	
2						434.78
3	13.33	0.12	7.36	7.36	7.36	
4	20.00	0.12	10.56	10.56	10.56	
5	14.17	0.12	7.65	7.65	7.65	

Tolerance for exceeding maximum shear or principal compression stress 0.0200

05-ΔΙΥΛΙΣΗ
 ULS design beams

Selected Beam Elements

FROM TO INC X-VALUE NC MEMBER CS0 CS1 CS2 CS3 CS4 CS5
 all elements

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992) DUMMY

All moments will be smoothed out between face and support
 Reinforcement will be accounted for sectional values as defined in AQUA
 Reinforcements saved as design case LCR 11

Considered Load Cases

201 202

Ultimate Load Design

=====

Design for ultimate loads EuroNorm EN 1992 (2004) Concrete Structures
 Biaxial bending

Safety factors	SC-1	SC-2	SC-S	SS-1	SS-2	SS-S	PIIa
	1.50	1.50	1.50	1.15	1.15	1.00	7
Strain limits	C1	C2	S1	S2	Z1	Z2	
max	-3.50	-2.00	δ= 1.00	45.00	-3.50	20.00	

parameters for reinforcements

Minimum reinforcements	compression	min. reinforcement	maximum-
Bending. Compress.	e/d	N/Npl	requ. section
0.13 [o/o]	0.20 [o/o]	3.50	0.0010
		0.00	0.10
			8.00

Tensile forces in the longitudinal reinforcements due to shear are NOT accounted for.

Material of sections uses Ultimate Limit strain-stress law with individual safety factors
 Material of reinforcements uses Ultimate Limit strain-stress law with individual safety factors

MNo.	temp lev.	Material-safety [-]	max.compr stress [MPa]	at strain [o/oo]	max.tens stress [MPa]	at strain [o/oo]	tension-stiffening [MPa]
1	0	1.500	-14.17	-2.00	0.00	0.00	
2	0	1.150	-500.00	-75.00	500.00	75.00	
3	0	1.500	-13.33	-2.00	0.00	0.00	
4	0	1.500	-20.00	-2.00	0.00	0.00	
5	0	1.500	-14.17	-2.00	0.00	0.00	

Shear Design

=====

Design for shear Eurocode EN 1992 (2004)

Minimum shear factor or tan of inclination of compressive struts 0.40 / 1.00

MNo	f-cd [MPa]	tau-rd [MPa]	sigIIQ [MPa]	sigIIIT [MPa]	sigIIQ+T [MPa]	fyd [MPa]
1	14.17	0.12	7.65	7.65	7.65	
2						434.78
3	13.33	0.12	7.36	7.36	7.36	
4	20.00	0.12	10.56	10.56	10.56	
5	14.17	0.12	7.65	7.65	7.65	

Tolerance for exceeding maximum shear or principal compression stress 0.0200

05-ΔΙΥΛΙΣΗ
 CRACK CONTROL W<0.30mm BEAMS

Selected Beam Elements

FROM	TO	INC	X-VALUE	NC	MEMBER	CS0	CS1	CS2	CS3	CS4	CS5
all elements											

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992)DUMMY

All moments will be smoothed out between face and support
 Reinforcement will be accounted for sectional values as defined in AQUA
 Reinforcements saved as design case LCR 12

Considered Load Cases

301

Ultimate Load Design

Design for unmanufactured loads EuroNorm EN 1992 (2004) Concrete Structures
 Biaxial bending

Safety factors	SC-1	SC-2	SC-S	SS-1	SS-2	SS-S	PIIa
	1.50	1.50	1.50	1.15	1.15	1.10	7
Strain limits	C1	C2	S1	S2	Z1	Z2	
max	-3.50	-2.00	3.00	10.00	-3.50	10.00	

parameters for reinforcements

Minimum reinforcements	compression	e/d	N/Npl	min. reinforcem.	maximum-	
Bending.	Compress.			requ. section	reinforc.	
0.00 [o/o]	0.30 [o/o]	3.50	0.0010	0.00	0.15	8.00

Tensile forces in the longitudinal reinforcements due to shear are NOT accounted for.

Material of sections uses Ultimate Limit strain-stress law with individual safety factors
 Material of reinforcements uses Ultimate Limit strain-stress law with individual safety factors

MNo.	temp lev.	Material-safety	max.compr stress	at strain	max.tens stress	at strain	tension-stiffening
		[-]	[MPa]	[o/oo]	[MPa]	[o/oo]	[MPa]
1	0	1.500	-14.17	-2.00	0.00	0.00	
2	0	1.150	-500.00	-75.00	500.00	75.00	
3	0	1.500	-13.33	-2.00	0.00	0.00	
4	0	1.500	-20.00	-2.00	0.00	0.00	
5	0	1.500	-14.17	-2.00	0.00	0.00	

Parameters for nonlinear stresses

Iteration for all forces and moments

Material of sections uses Serviceability strain-stress law without safety factors
 Material of reinforcements uses Serviceability strain-stress law without safety factors

MNo.	temp lev.	Material-safety	max.compr stress	at strain	max.tens stress	at strain	tension-stiffening
		[-]	[MPa]	[o/oo]	[MPa]	[o/oo]	[MPa]
1	0	1.000	-33.00	-2.07	0.00	0.00	
2	0	1.000	-575.00	-75.00	575.00	75.00	
3	0	1.000	-28.00	-1.97	0.00	0.00	
4	0	1.000	-38.00	-2.16	0.00	0.00	
5	0	1.000	-33.00	-2.07	0.00	0.00	

Interaction thin walled normal- and shearstress via Prandtl flow rule

05-ΔΙΥΛΙΣΗ
 ULS design beams

Selected Beam Elements

FROM	TO	INC	X-VALUE	NC	MEMBER	CS0	CS1	CS2	CS3	CS4	CS5
all elements											

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992) DUMMY

All moments will be smoothed out between face and support
 Reinforcement will be accounted for sectional values as defined in AQUA
 Reinforcements saved as design case LCR 20

Considered Load Cases

101	102	103	104	201	202
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Ultimate Load Design

=====

Design for ultimate loads EuroNorm EN 1992 (2004) Concrete Structures
 Biaxial bending

Safety factors	SC-1	SC-2	SC-S	SS-1	SS-2	SS-S	PIIa
	1.50	1.50	1.50	1.15	1.15	1.00	7
Strain limits	C1	C2	S1	S2	Z1	Z2	
max	-3.50	-2.00	δ= 1.00	45.00	-3.50	20.00	

parameters for reinforcements

Minimum reinforcements	compression	min. reinforcem.	maximum-
Bending. Compress.	e/d	N/Npl	requ. section
0.13 [o/o]	0.20 [o/o]	3.50	0.0010
		0.00	0.10
			8.00

Tensile forces in the longitudinal reinforcements due to shear are NOT accounted for.

Material of sections uses Ultimate Limit strain-stress law with individual safety factors
 Material of reinforcements uses Ultimate Limit strain-stress law with individual safety factors

MNo.	temp lev.	Material-safety [-]	max.compr stress [MPa]	at strain [o/oo]	max.tens stress [MPa]	at strain [o/oo]	tension-stiffening [MPa]
1	0	1.500	-14.17	-2.00	0.00	0.00	
2	0	1.150	-500.00	-75.00	500.00	75.00	
3	0	1.500	-13.33	-2.00	0.00	0.00	
4	0	1.500	-20.00	-2.00	0.00	0.00	
5	0	1.500	-14.17	-2.00	0.00	0.00	

Shear Design

=====

Design for shear Eurocode EN 1992 (2004)
 Minimum shear factor or tan of inclination of compressive struts 0.40 / 1.00

MNo	f-cd [MPa]	tau-rd [MPa]	sigIIQ [MPa]	sigIIIT [MPa]	sigIIQ+T [MPa]	fyd [MPa]
1	14.17	0.12	7.65	7.65	7.65	
2						434.78
3	13.33	0.12	7.36	7.36	7.36	
4	20.00	0.12	10.56	10.56	10.56	
5	14.17	0.12	7.65	7.65	7.65	

Tolerance for exceeding maximum shear or principal compression stress 0.0200

05-ΔΙΥΛΙΣΗ
 CRACK CONTROL W<0.30mm BEAMS

Selected Beam Elements

FROM	TO	INC	X-VALUE	NC	MEMBER	CS0	CS1	CS2	CS3	CS4	CS5
all elements											

Default design code is EuroNorm EN 1992 (2004) Concrete Structures (Europe) V 30.0
 Structure and Tab.7.1N: AN (Buildings)
 Snow load zone : 1

Materials

- No. 1 C 25/30 (EN 1992)
- No. 2 B 500 C (EN 1992)
- No. 3 C 20/25 (EN 1992)
- No. 4 C 30/37 (EN 1992)
- No. 5 C 25/30 (EN 1992)DUMMY

All moments will be smoothed out between face and support
 Reinforcement will be accounted for sectional values as defined in AQUA
 Reinforcements saved as design case LCR 21
 Reinforcements superposed with existing design case LCR 20

Considered Load Cases

301

Ultimate Load Design

=====

Design for unmanufactured loads EuroNorm EN 1992 (2004) Concrete Structures

Biaxial bending

Safety factors	SC-1	SC-2	SC-S	SS-1	SS-2	SS-S	PIIa
	1.50	1.50	1.50	1.15	1.15	1.10	7
Strain limits	C1	C2	S1	S2	Z1	Z2	
max	-3.50	-2.00	3.00	10.00	-3.50	10.00	

parameters for reinforcements

Minimum reinforcements	compression	min. reinforcement	maximum-
Bending. Compress.	e/d	N/Npl	requ. section reinforc.
0.00 [o/o]	0.30 [o/o]	3.50	0.0010
		0.00	0.15
			8.00

Tensile forces in the longitudinal reinforcements due to shear are NOT accounted for.

Material of sections uses Ultimate Limit strain-stress law with individual safety factors
 Material of reinforcements uses Ultimate Limit strain-stress law with individual safety factors

MNo.	temp lev.	Material-safety [-]	max.compr stress [MPa]	at strain [o/oo]	max.tens stress [MPa]	at strain [o/oo]	tension-stiffening [MPa]
1	0	1.500	-14.17	-2.00	0.00	0.00	
2	0	1.150	-500.00	-75.00	500.00	75.00	
3	0	1.500	-13.33	-2.00	0.00	0.00	
4	0	1.500	-20.00	-2.00	0.00	0.00	
5	0	1.500	-14.17	-2.00	0.00	0.00	

Parameters for nonlinear stresses

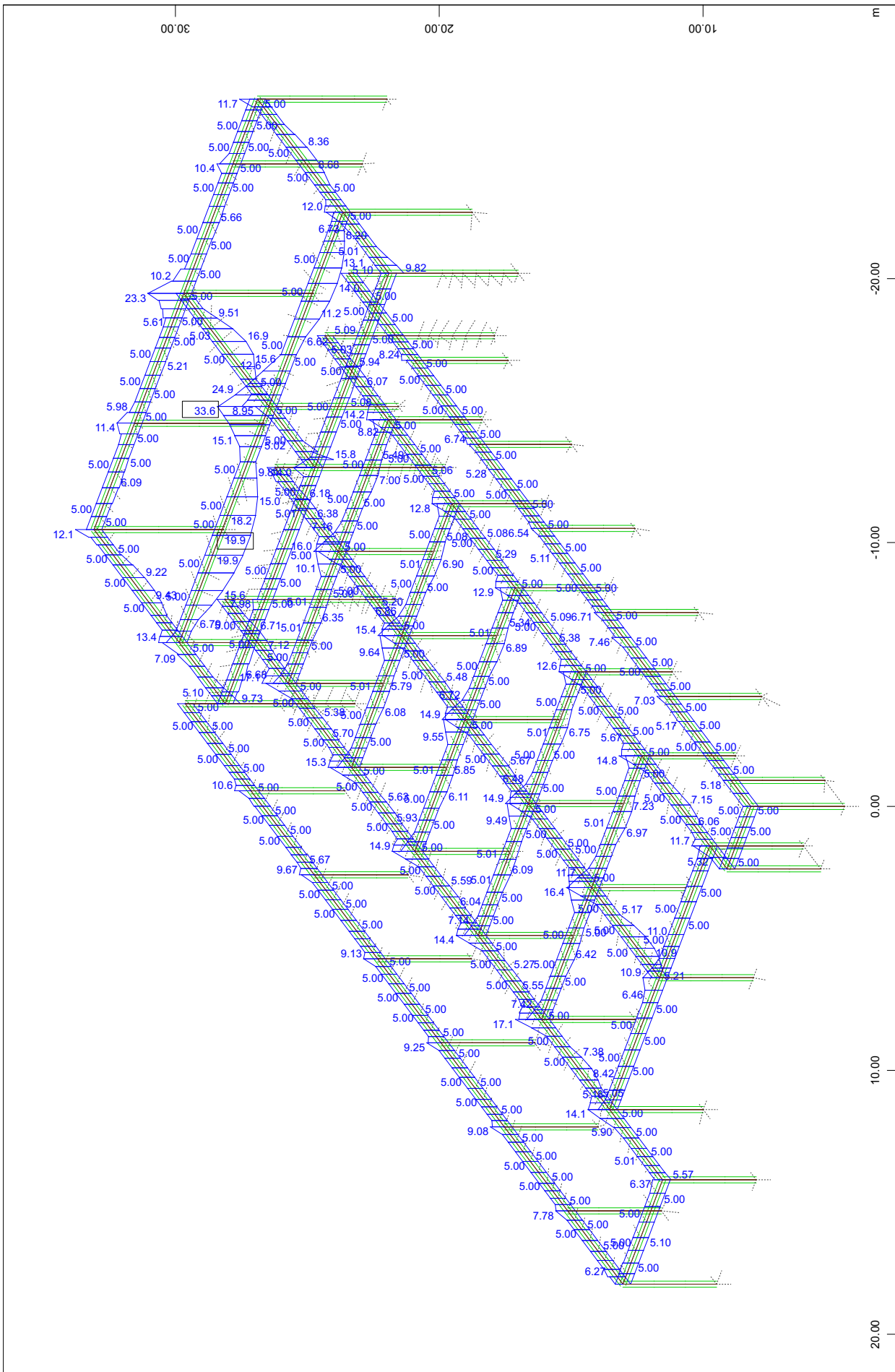
Iteration for all forces and moments

Material of sections uses Serviceability strain-stress law without safety factors
 Material of reinforcements uses Serviceability strain-stress law without safety factors

MNo.	temp lev.	Material-safety [-]	max.compr stress [MPa]	at strain [o/oo]	max.tens stress [MPa]	at strain [o/oo]	tension-stiffening [MPa]
1	0	1.000	-33.00	-2.07	0.00	0.00	
2	0	1.000	-575.00	-75.00	575.00	75.00	
3	0	1.000	-28.00	-1.97	0.00	0.00	
4	0	1.000	-38.00	-2.16	0.00	0.00	
5	0	1.000	-33.00	-2.07	0.00	0.00	

Interaction thin walled normal- and shearstress via Prandtl flow rule

05-ΔΙΥΛΙΣΗ
ΠΕΡΙΒΑΛΛΟΥΣΑ ΟΠΛΙΣΜΩΝ ΔΟΚΩΝ ΟΡΟΦΗΣ (LCR 2)



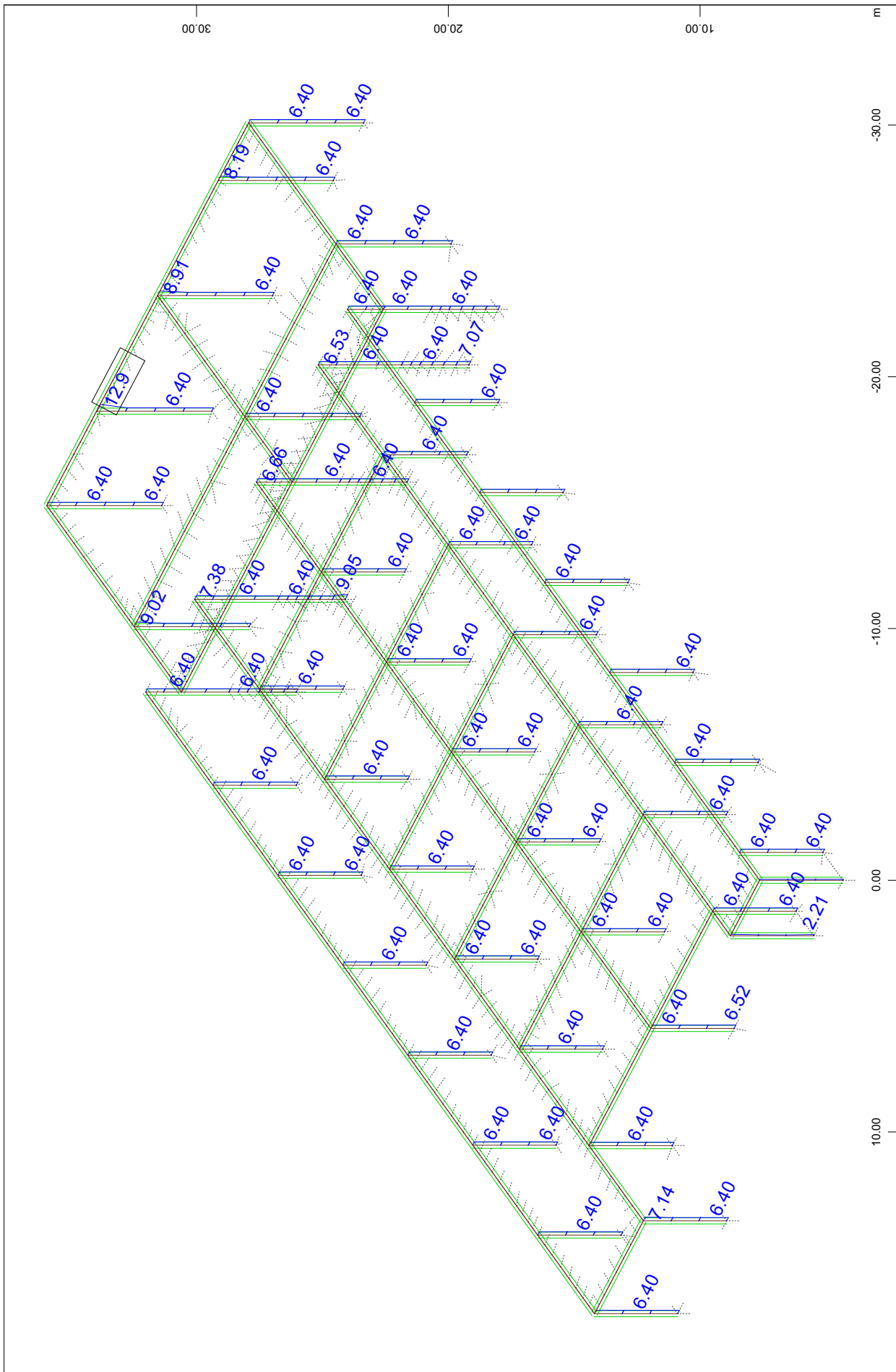
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M 1 : 207
X * 0.725
Y * 0.872
Z * 0.845

Sector of system Group 1
Beam Elements , Longitudinal Reinforcements Lay. 1, Design Case 21 , 1 cm 3D = 30.0 cm2 (Max=19.9)
Beam Elements , Longitudinal Reinforcements Lay. 2, Design Case 21 , 1 cm 3D = 30.0 cm2 (Max=33.6)

X
Y Z

05-ΔΙΥΛΙΣΗ
 ΟΠΛΙΣΜΟΙ ΥΠΟΣΤΥΛΩΜΑΤΩΝ ΟΚΑ (LCR 10)



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M 1 : 217
 X * 0.801
 Y * 0.859
 Z * 0.787

Sector of system Group 1
 Beam Elements , Longitudinal Reinforcements Lay. 0, Design Case 10 , 1 cm 3D = 80.0 cm2 (Max=12.9)

Y Z X

05-ΔΙΥΛΙΣΗ
ΟΠΛΙΣΜΟΙ ΥΠΟΣΤΥΛΩΜΑΤΩΝ ΣΕΙΣΜΟΣ (LCR 11)

